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# **Microwave reflectometry diagnostic for density profile and fluctuation measurements on Helically Symmetric eXperiment (HSX)**

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# Outline



- **Introduction**
- **Observations of density fluctuation**
- **Profile reconstruction with O-mode regime**
- **Plan of system renovation**
- **summary**



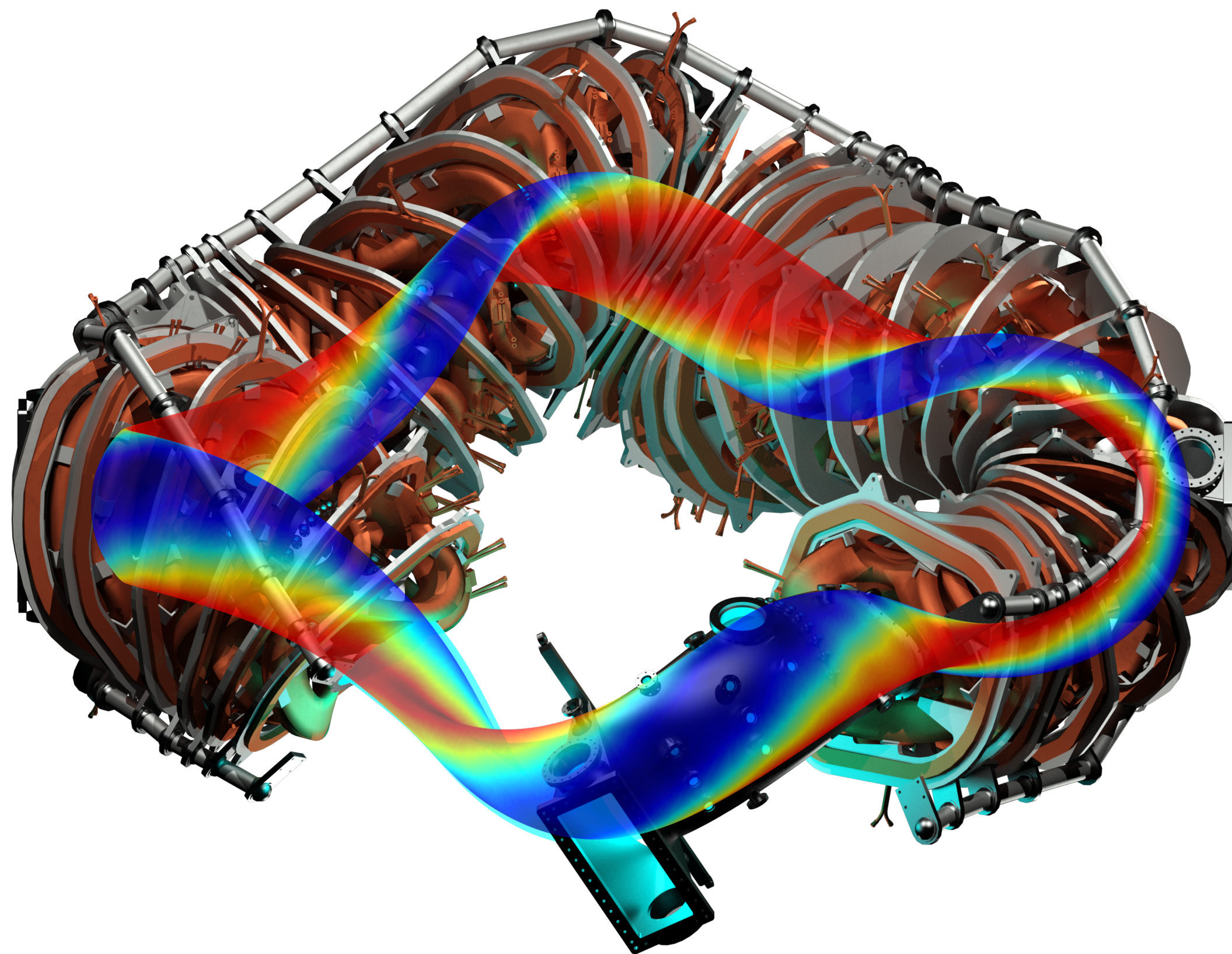
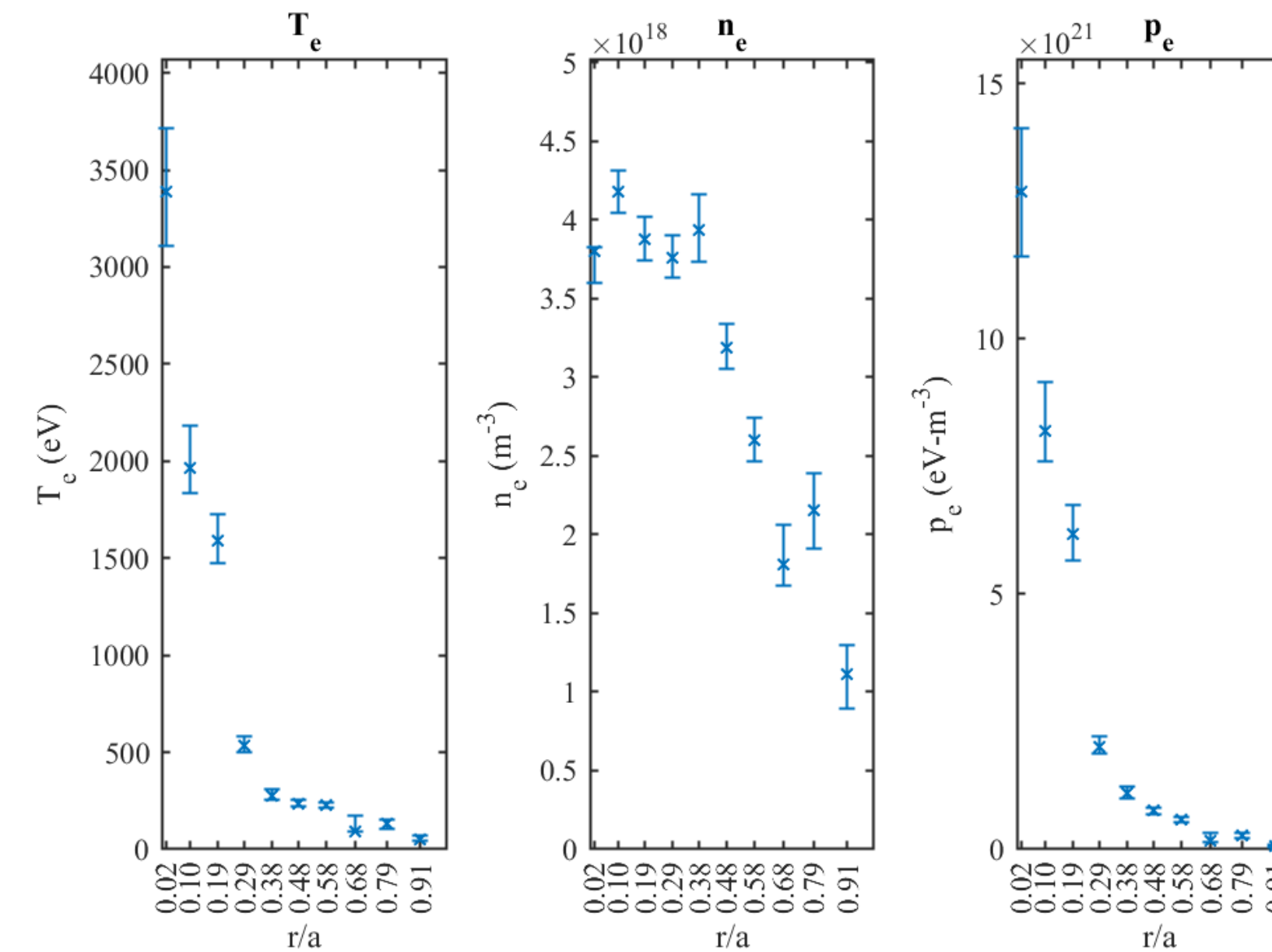


# HSX is an ideal testbed for studies of micro-instabilities and neoclassical transport



- Helically Symmetric eXperiment (HSX) is featured a quasi-helically symmetric magnetic configurations (QHS)
- 4 field periods (48 modular + 48 planar coils)
- rotational transform  $\iota > 1$

Shot #43, 2024-04-03, t = 40 ms



Radius	$R/a = 1.2 \text{ m}/0.12 \text{ m}$
ECRH	@28 GHz $P_{\text{absorption}} \sim 20 \text{ kW}$
Pulse length	50 ms
On-axis B field	0.5~1.0 T
Core temperature	$T_e \leq 3 \text{ keV}$ $T_i \sim 50 \text{ eV}$
Plasma density	$\sim 10^{13} \text{ cm}^{-3}$
Diagnostics	<b>Reflectometry</b> , CECE, TS, Interferometer, fast camera, Mirnov coils, CHER ...

<https://hsx.wisc.edu/>

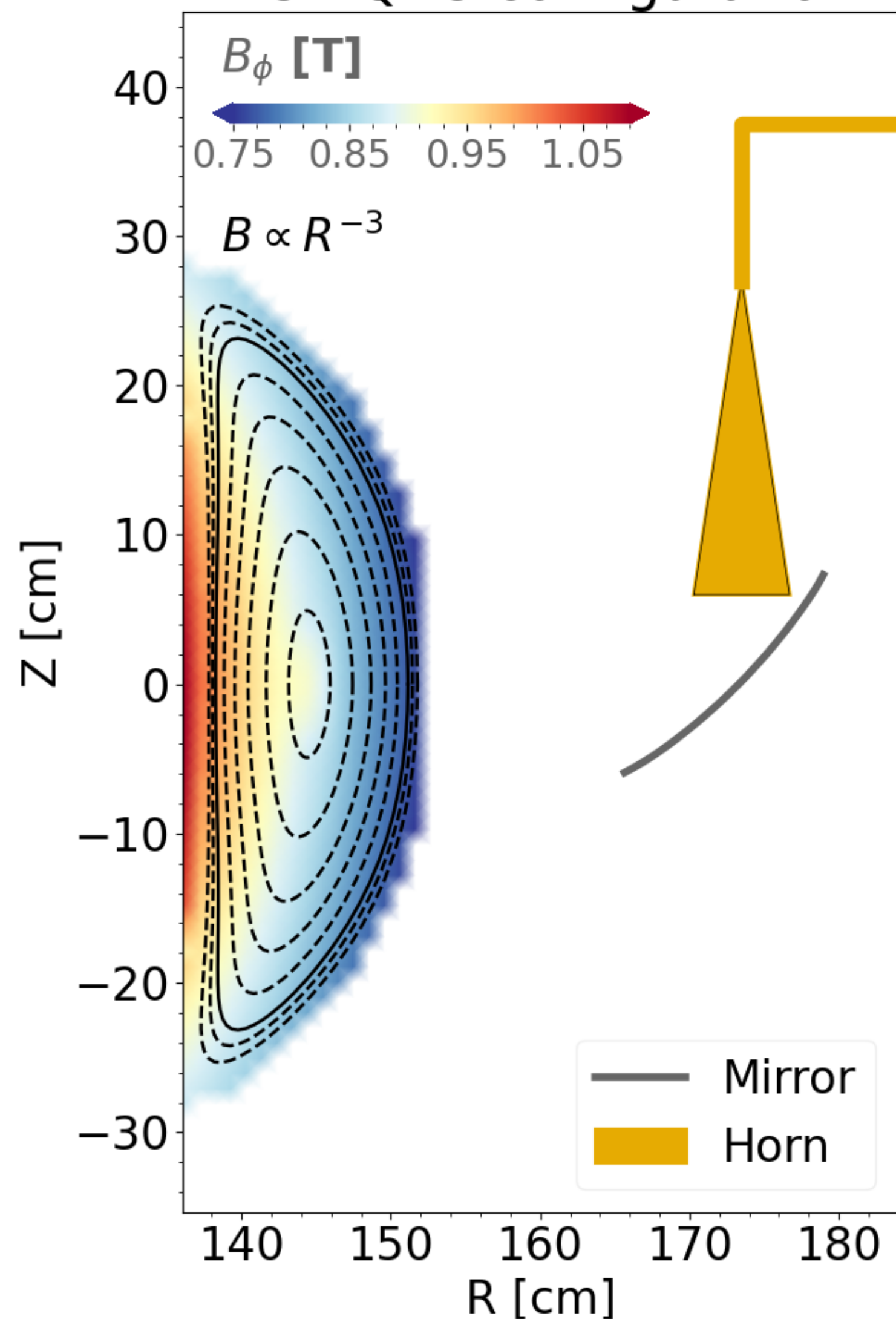




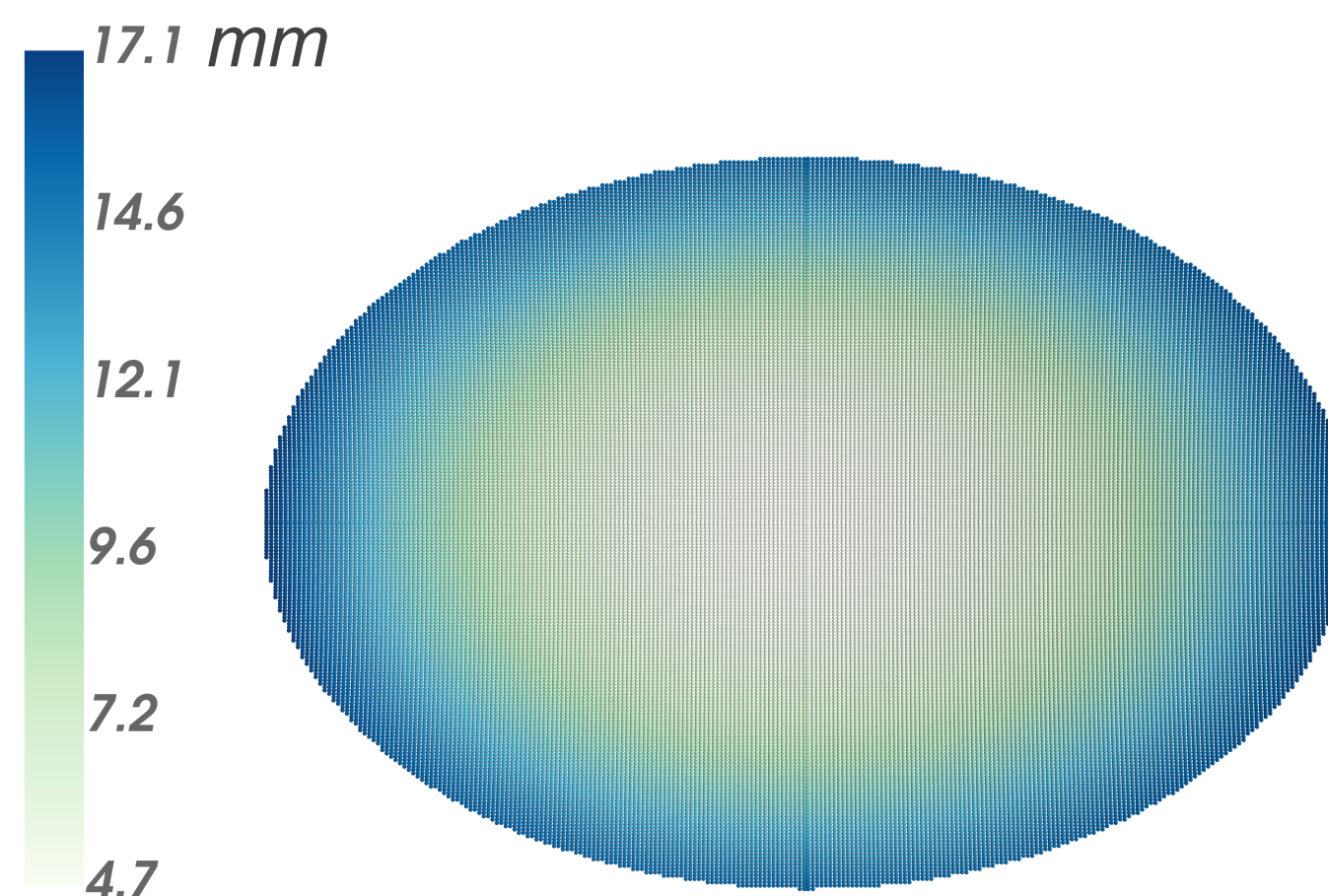
# Reflectometry is designed to measure the electron density fluctuation and profile



HSX QHS configuration



- Monostatic horn at boxport A
  - Major radius at 173.5 cm
  - E-plane 63.5 mm / H-plane 88.5 mm
  - L = 210 mm
  - Waveguide: WR-42
- Vertically-installed horn, facing toward an elliptical mirror at equatorial plane



- Elliptical mirror
  - Distance to the horn 60 mm
  - Focal length 143.16 mm (E-plane), 137.89 mm (H-plane)
  - Incident angle  $45^\circ$

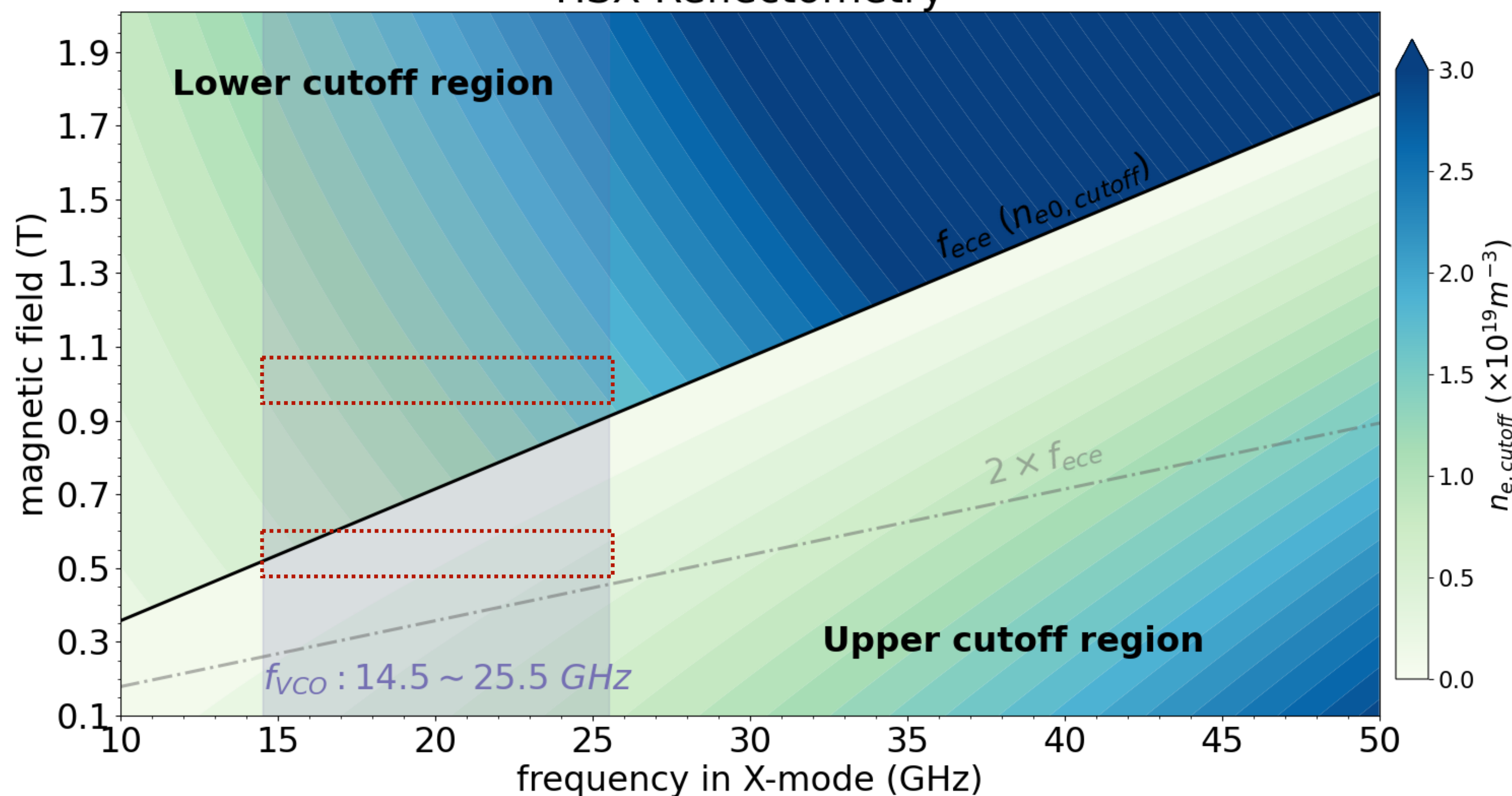




# Polarization is selected by rotating the mirror and horn



HSX Reflectometry



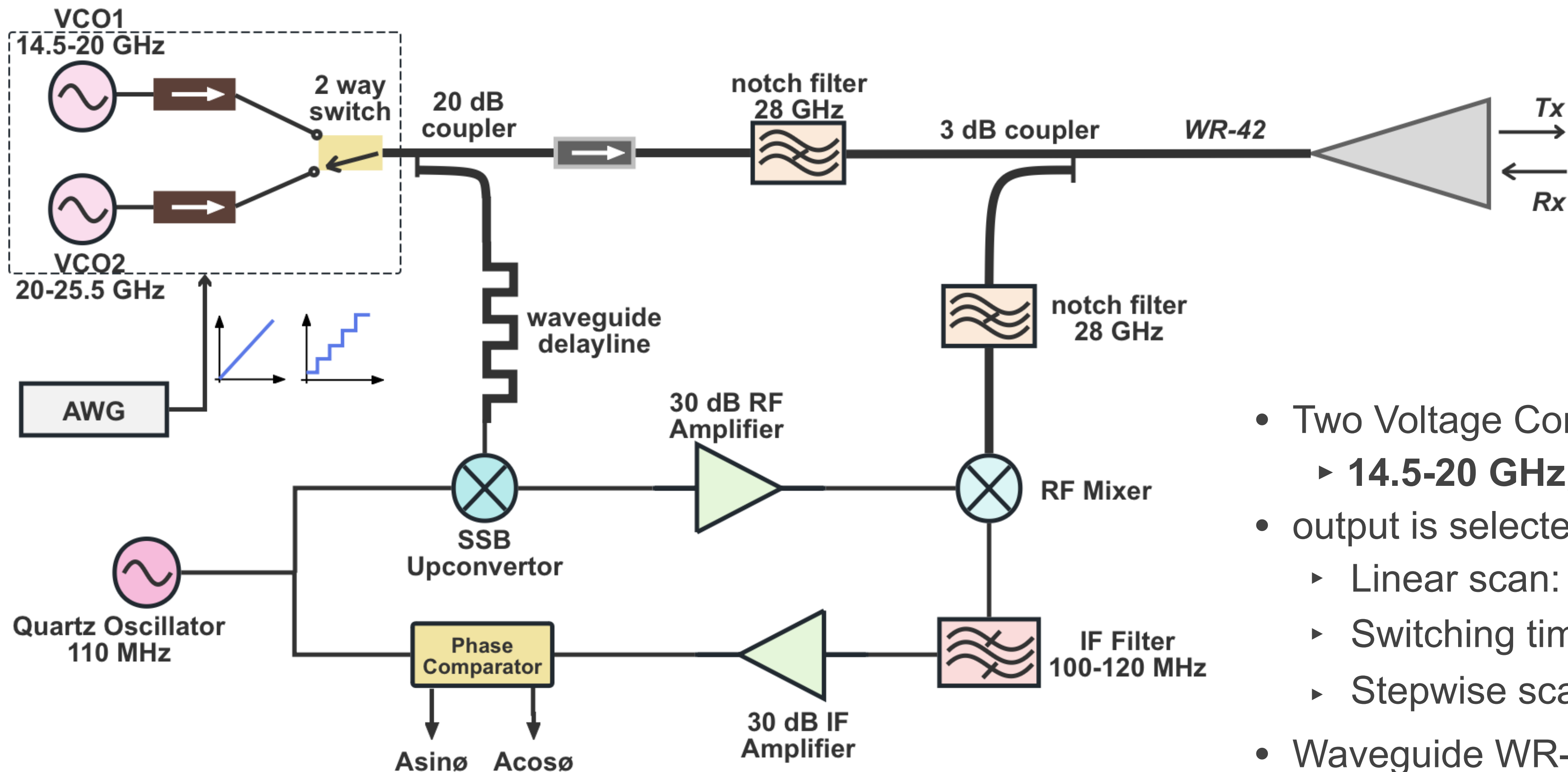
- Operational frequency range **14.5~25.5 GHz**
- O-mode** operation at  $B=1$  T, corresponding to cutoff density of  **$2.8 \sim 7 \times 10^{18} \text{ m}^{-3}$**
- X-mode** operation per requirement
  - upper cutoff at 0.5 T:  **$0.05 \sim 0.36 \times 10^{19} \text{ m}^{-3}$**
  - lower cutoff at 1 T:  **$0.72 \sim 1.7 \times 10^{19} \text{ m}^{-3}$**

$$|B| \propto R^{-3}$$





# Layout of microwave components: Conventional FMCW heterodyne system

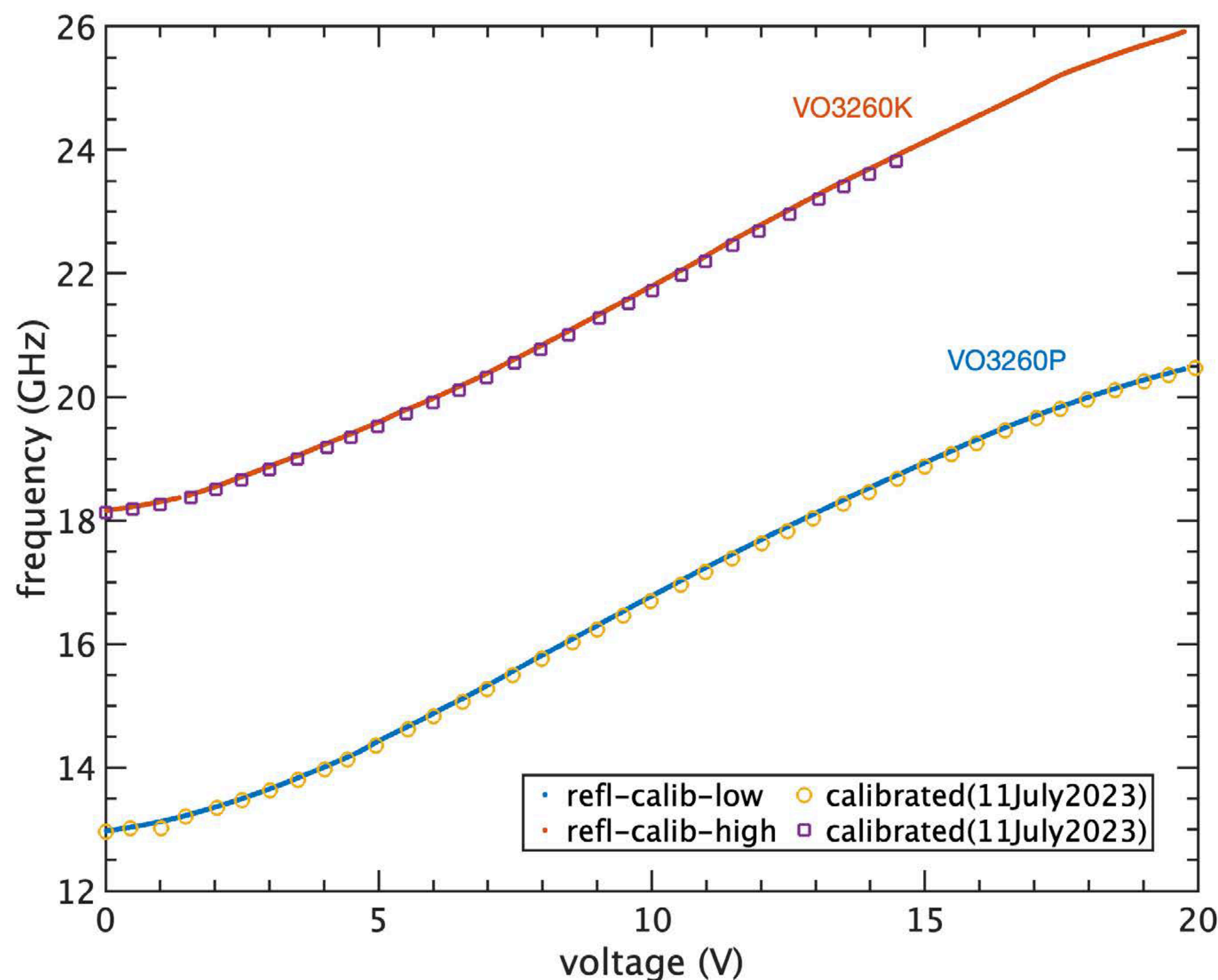


- Two Voltage Control Oscillators (VCO)
  - 14.5-20 GHz, 20-25.5 GHz
- output is selected by a fast-pin switch
  - Linear scan:  $df/dt \sim 27.7 \text{ GHz/ms}$
  - Switching time:  $\sim 54 \mu s$  (18.5~20 GHz)
  - Stepwise scan:  $N_f = 20, \Delta f = 500 \text{ MHz}$
- Waveguide WR-42 delayline  $\sim 10 \text{ m}$  to compensate the phase at LO of RF mixer





# VCOs are re-calibrated after the HSX refurbishment



- HSX was refurbished in 2023 for high density operation planned at late 2024
- Reflectometry system hasn't been operated for decades
- VCO performance is the same as before
- Frequency-voltage curve matched to the original values

- *Dots: original calibrated data*
- *Circle & rectangle: newly-calibrated data*





# Outline



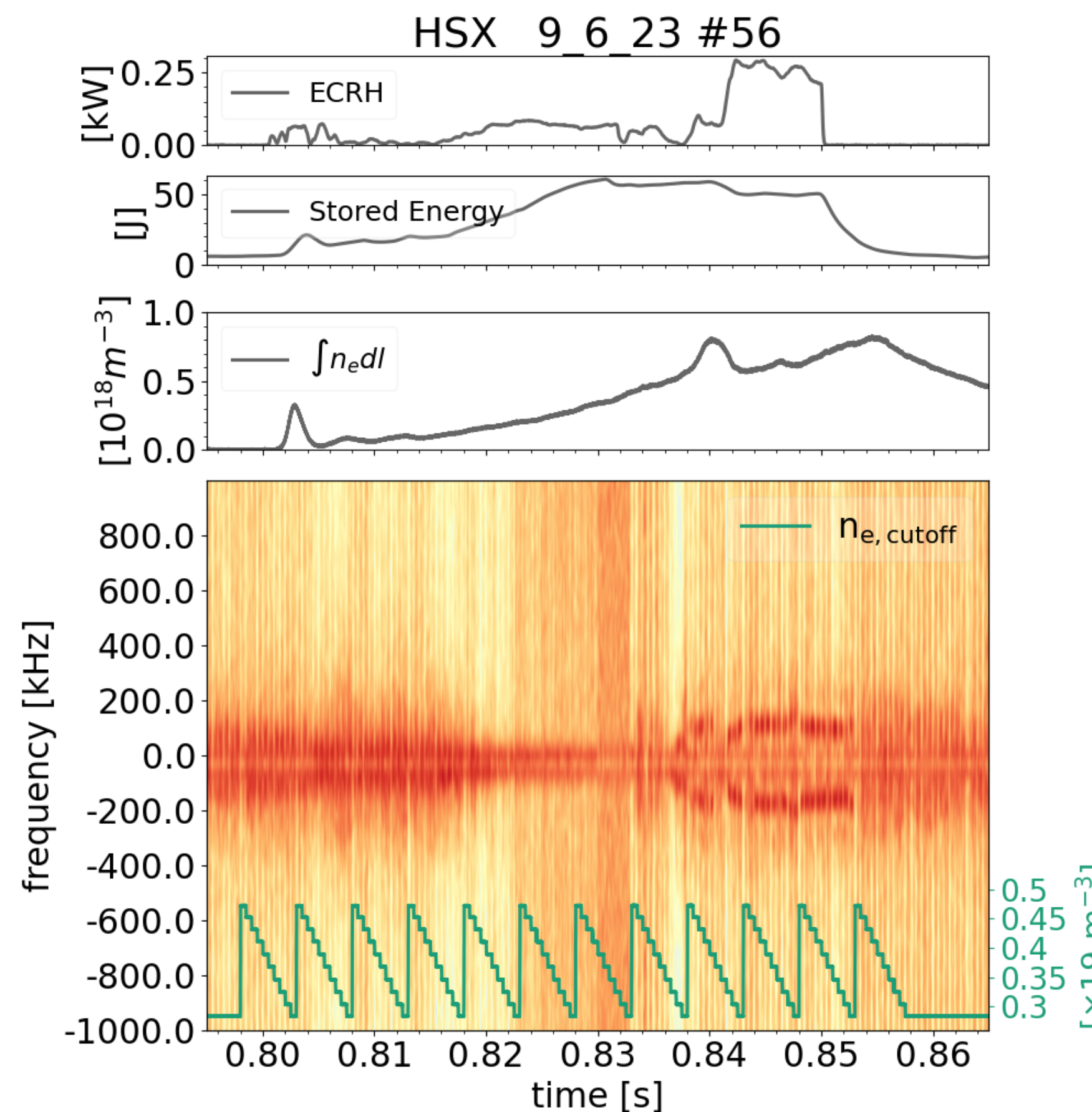
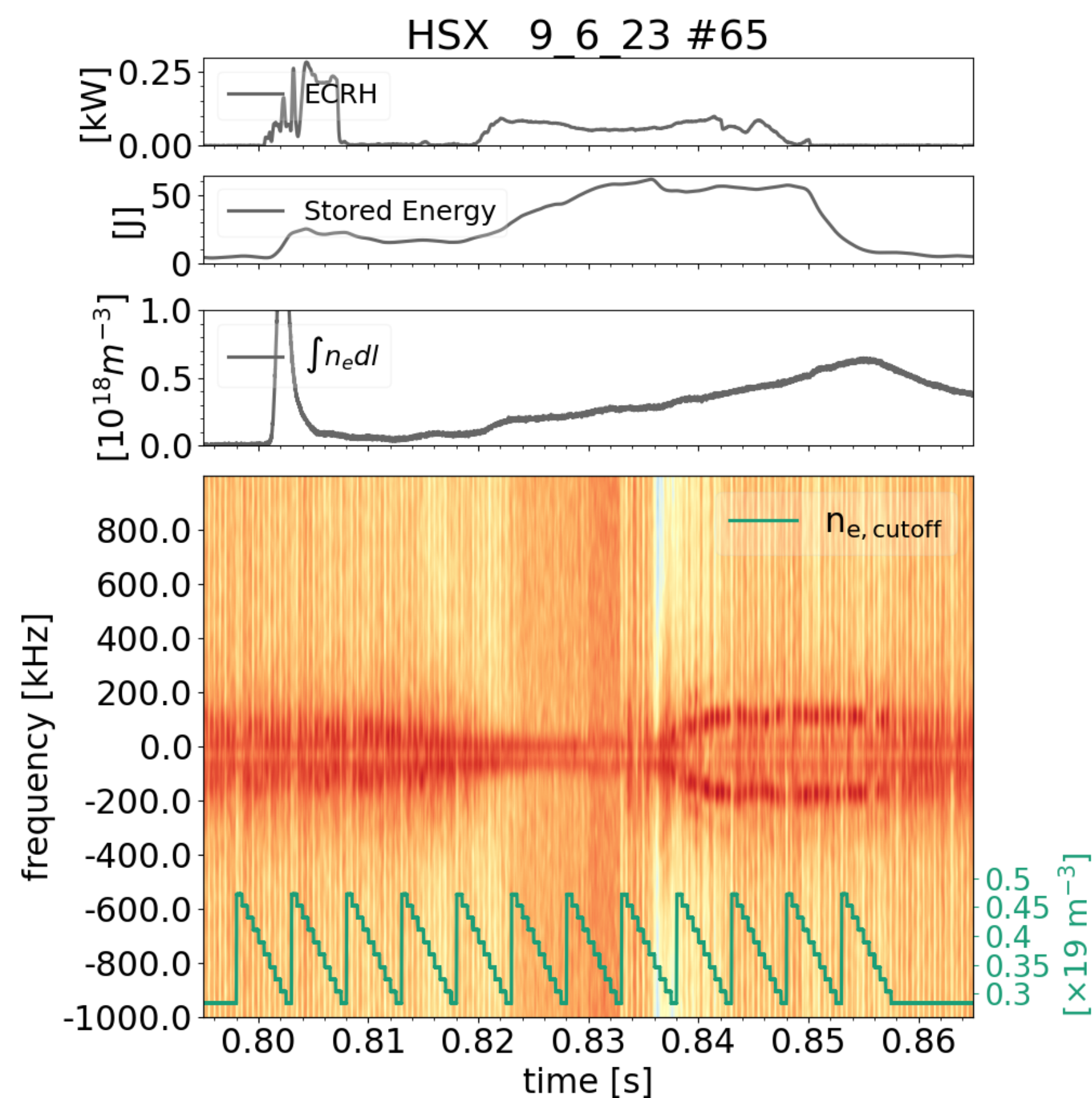
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# A turbulent mode observed during density ramping



- Mode frequency  $\sim 150$  kHz
- Appears after 0.835 s, remains the same at all cutoff density
- Could play a role on the profile gradient
- Not clear the mode behavior (electronic-magnetic mode?)



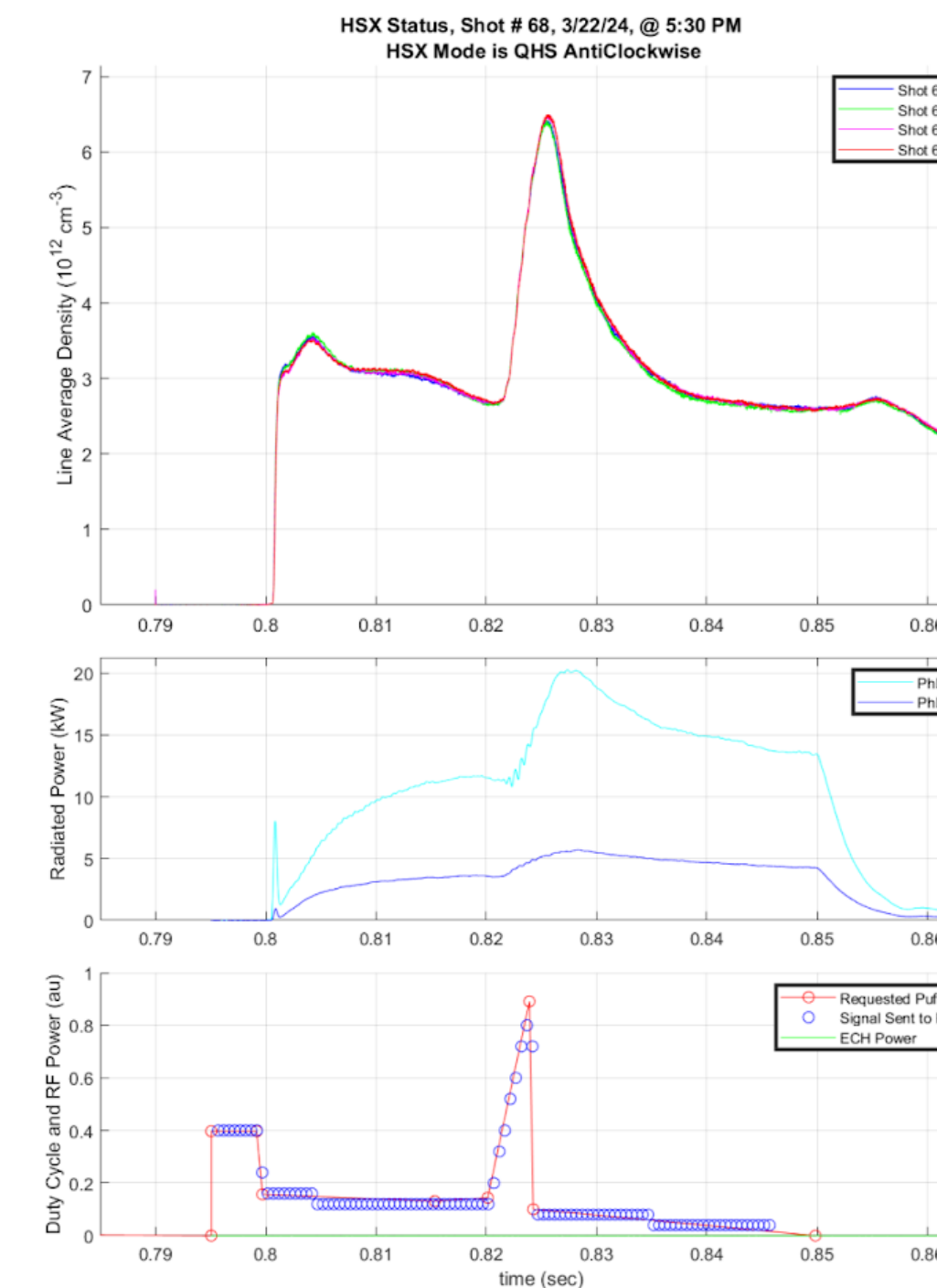
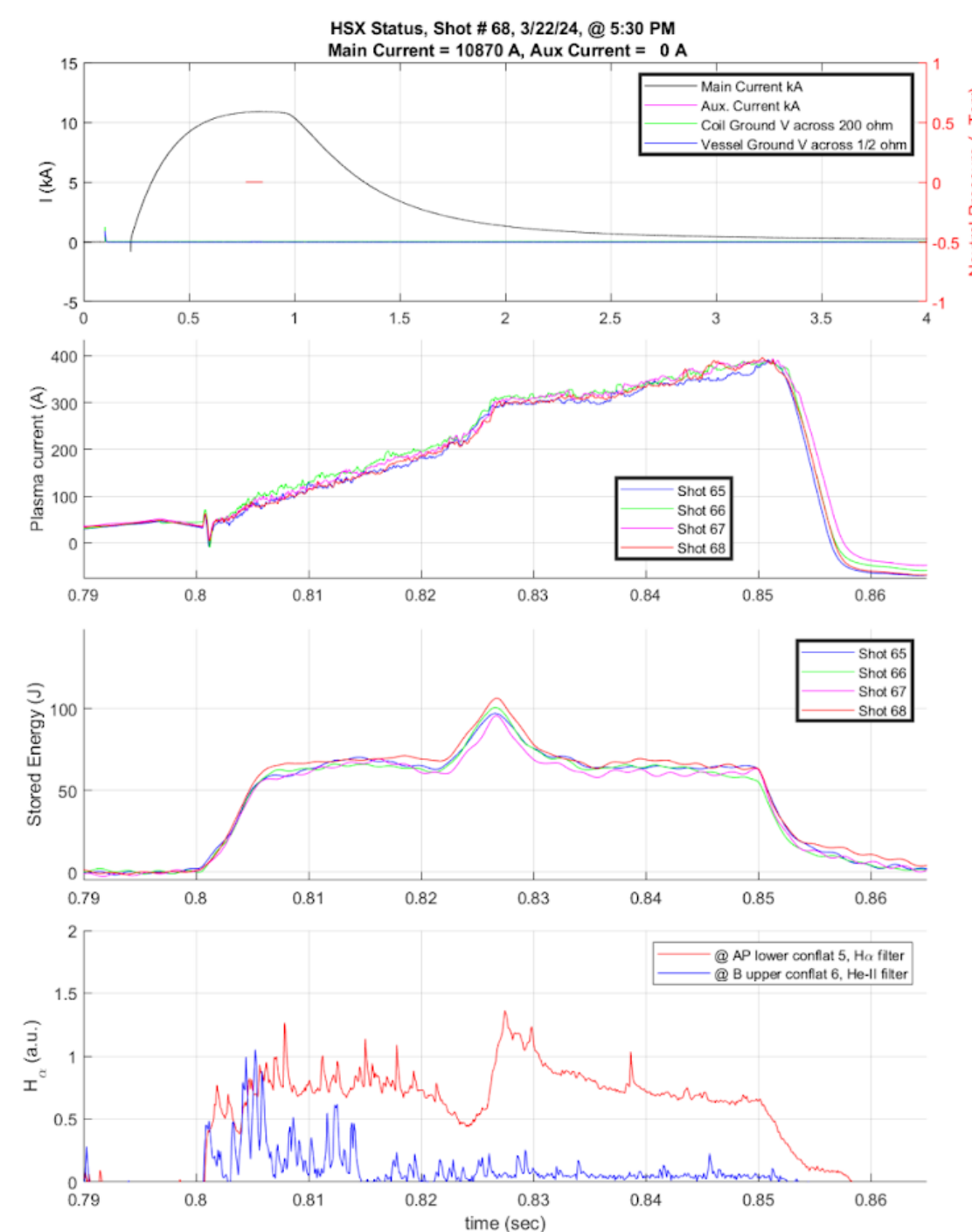
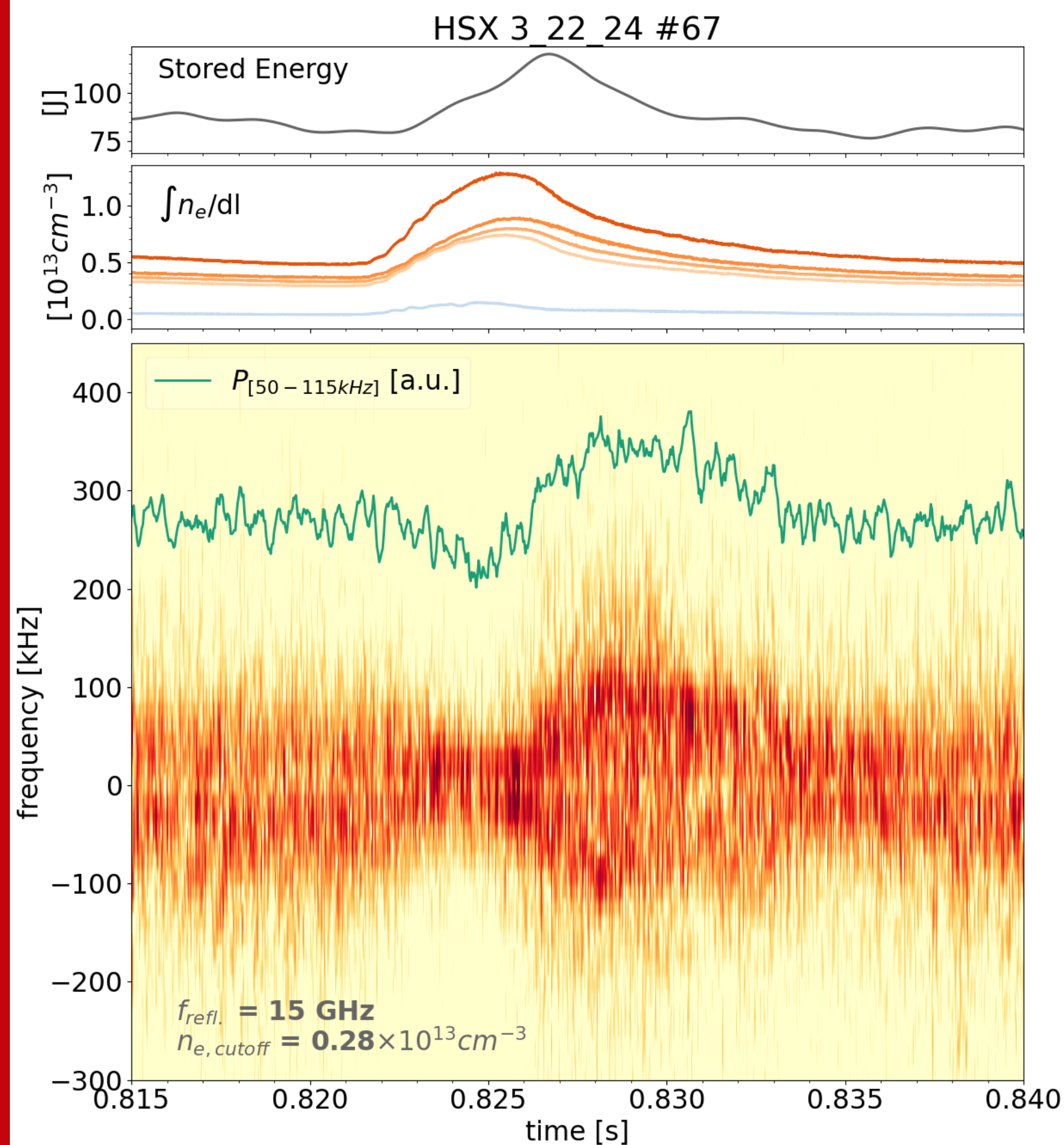




# Turbulence modulation is observed during the gas puffing experiment



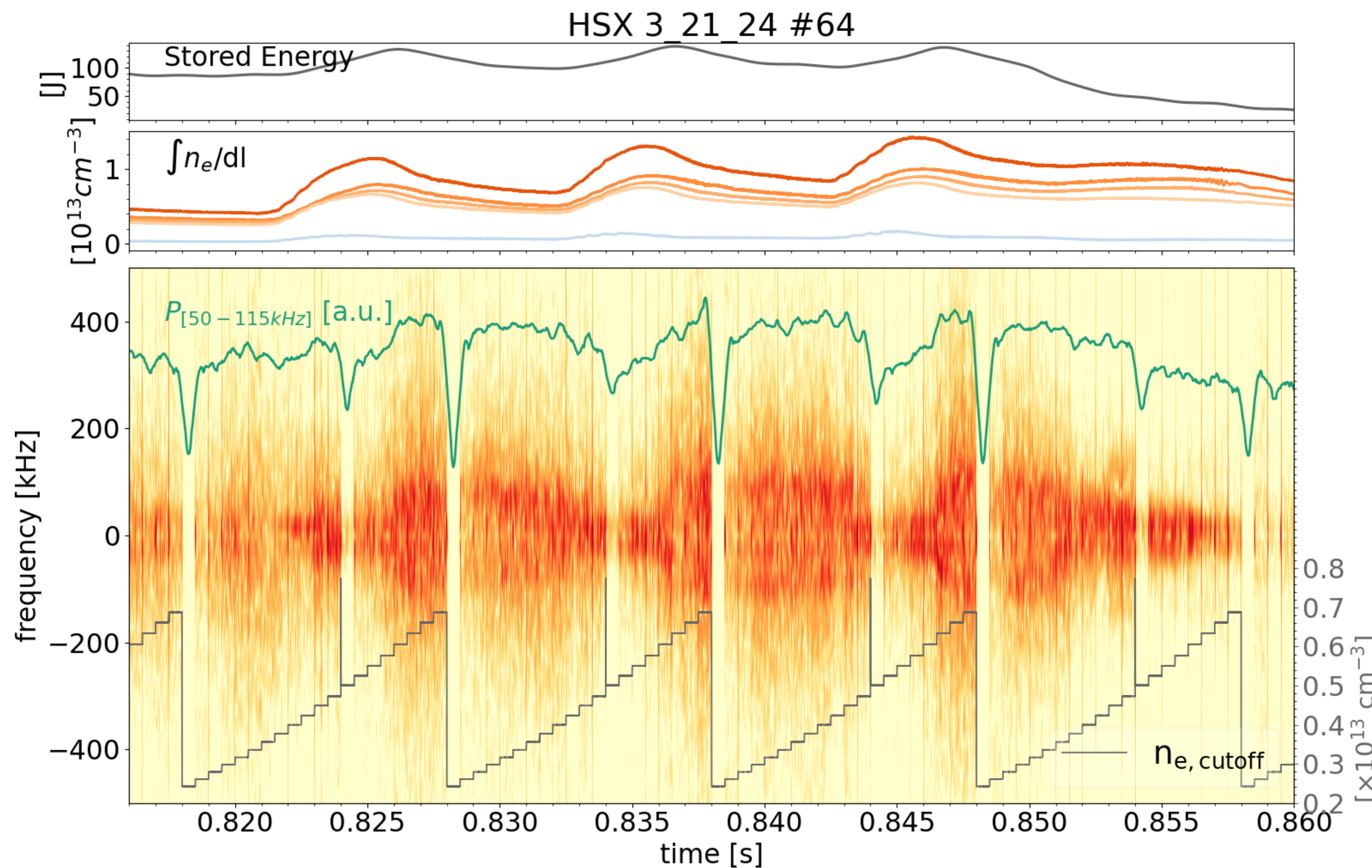
- Gas puffing is applied to modulate plasma density
- At ne rise, turbulence is suppressed (f < 50 kHz mode?)
- At ne decrease, spectral power integrated at 50-115 kHz
- Turbulence at 100 kHz appears at the late phase when the density decreases







# Radial location of 100 kHz turbulence is determined with stepwise scan



- 100 kHz turbulence regularly appear at the ne-decreasing phase in each gas-puff cycle
- Exist only when ne starts to decrease, yielding a relation between density gradient and the turbulence modulation
- Density profile is needed to confirm the radial coverage of the 100 kHz mode





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# Choi-William Distribution (CWD) is applied to extrapolate $f_{beat}$ from time-frequency spectrum



- For HSX reflectometer:  $f_s = 8 \text{ Msps}$ ,  $1/dt \approx 2.2 \text{ kHz}$ . CWD is applied to calculate the beat frequency spectrum
- CWD can improve the time-frequency resolution and suppress the cross-term interference or artifacts

$$P(n, \theta) = 2 \sum_{\tau=-\infty}^{\infty} h_N(\tau) \exp(-j2\theta\tau) \left[ \sum_{\mu=-\infty}^{\infty} h_M(\mu) \frac{\exp(-\mu^2\sigma/4\tau^2)}{(4\pi\tau^2/\sigma)^{0.5}} S(n + \mu + \tau) S^*(n + \mu - \tau) \right]$$

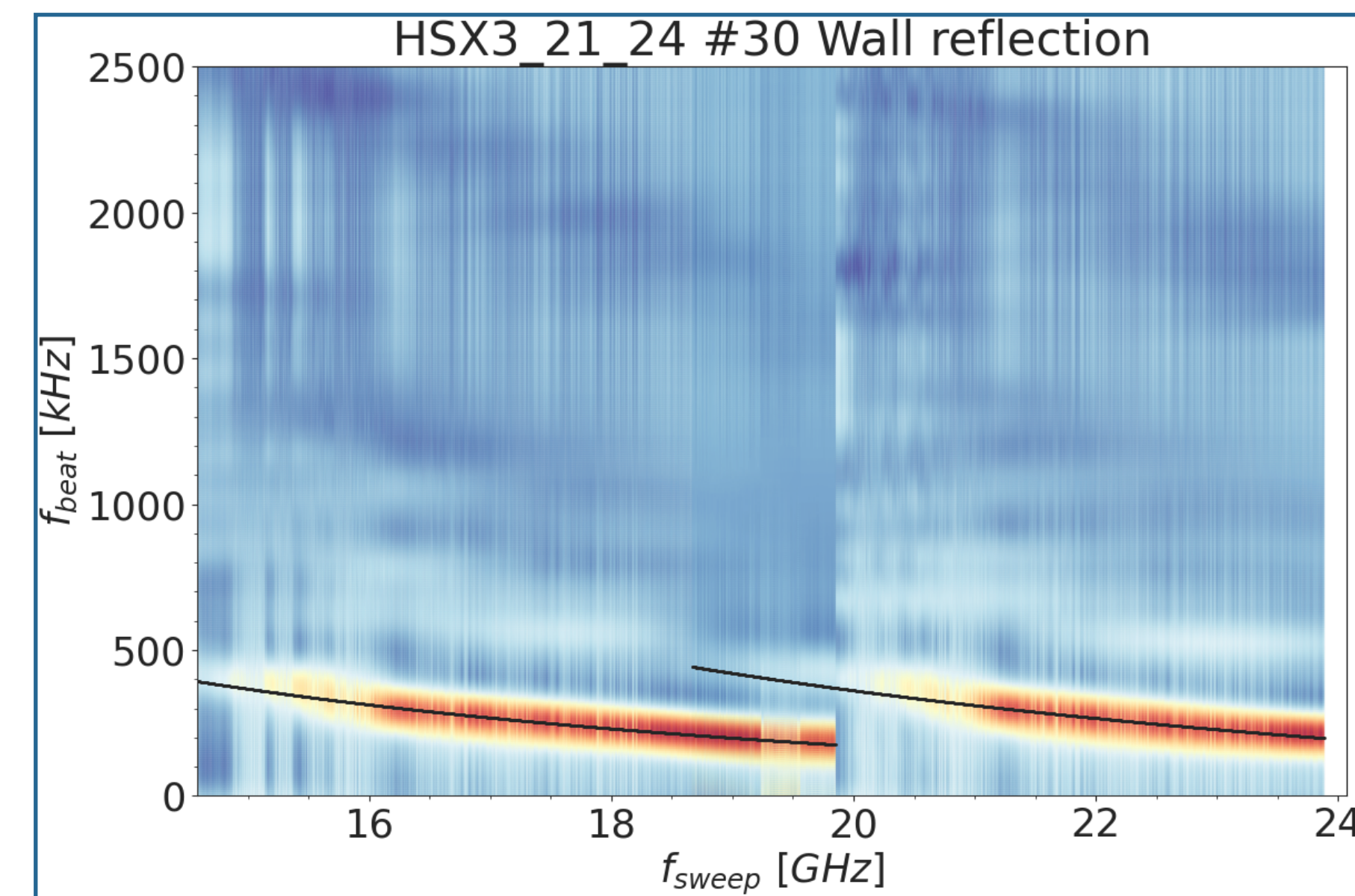
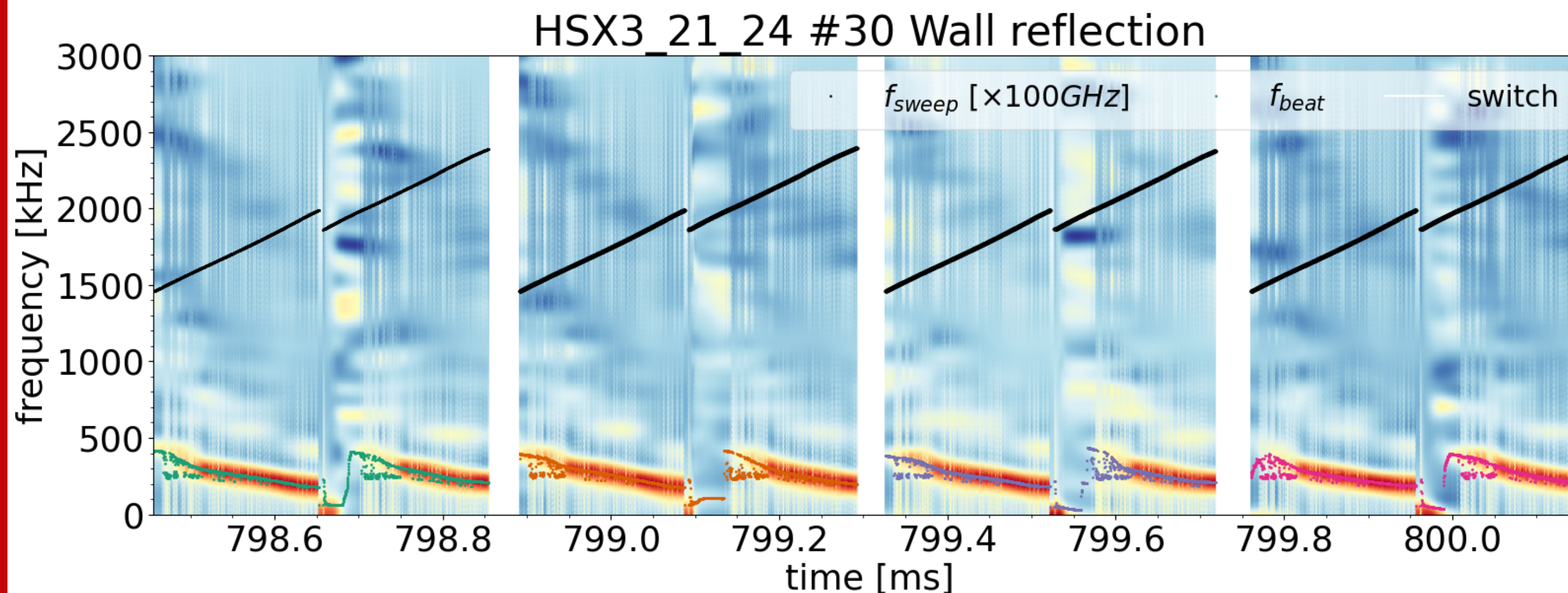
- Kernel is  $\phi(\xi, \tau) = \exp(-\xi^2\tau^2/\sigma)$ , where  $\sigma$  ( $\sigma > 0$ ) is scaling factor
- The time and frequency resolution is determined by  $h_N(\tau)$  and  $h_M(\mu)$  respectively
- $h_N(\tau)$  is a symmetrical window,  $h_M(\mu)$  determines the duration of the time indexed autocorrelation function
- CWD is more robust than the spectrogram especially when data volume is insufficient

H Choi, W Williams, IEEE Trans. Signal Process. 37, 862 (1989)





# Inner-wall reflected signal is measured as a reference of the system dispersion



- The first several cycles (before ECRH) are chosen, which are reflected from the inner wall
- Averaged  $f_{beat}$  spectrum is obtained, then the system delays are fit to the function:

$$f_{beat,wall} = a + b/(1 - f_{sweep})^{0.5}$$

- Parameters a, b are applied to calibrate the  $f_{beat}$  during plasma operation

Low-VCO:  $a = -1.99e+08$ ,  $b = 1.99e+08$

high-VCO:  $a = -4.36e+08$ ,  $b = 4.36e+08$

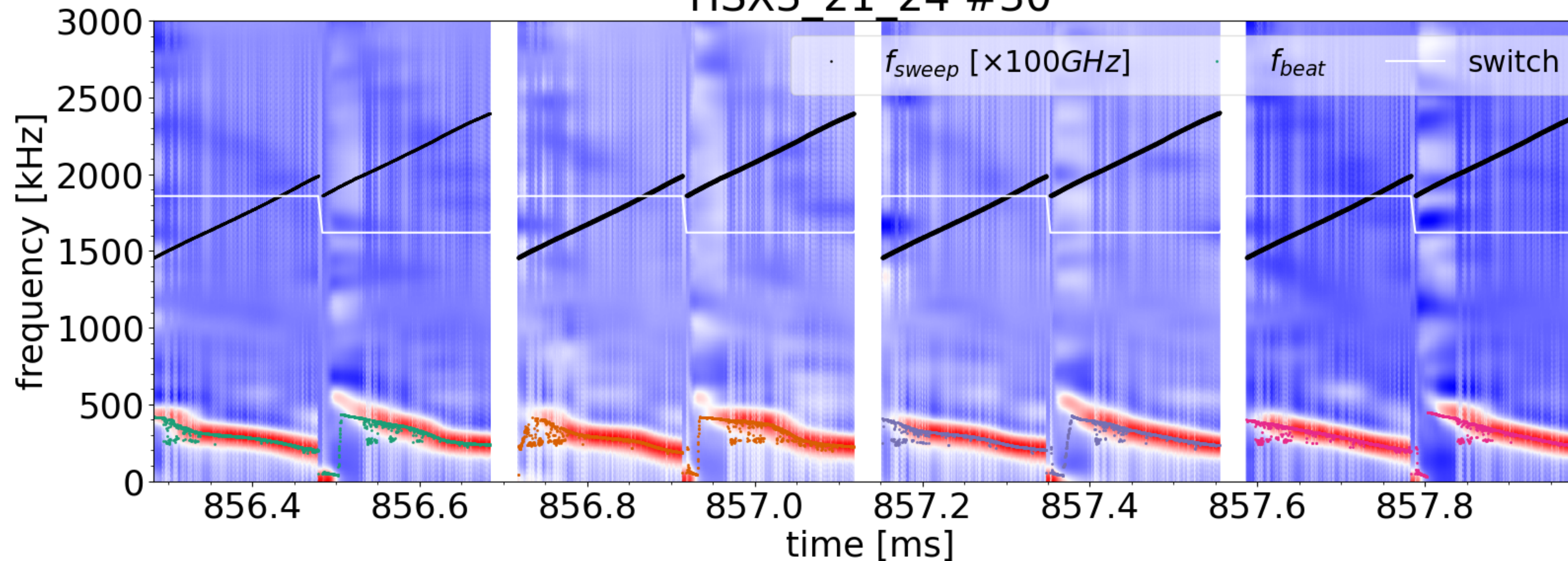




# $f_{beat}$ is obtained from the spectrum during plasma operation



HSX3 21 24 #30



- Sweeping rate  $1/dt = 2.2 \text{ kHz}$ ,  $f_{beat} = 100 \sim 300 \text{ kHz}$

- For the O-mode,  $f_{beat} = (\tau_{plasma} + \tau_{sys}) \frac{df_{VCO}}{dt}$

$$f_{beat,wall} = (\tau_0 + \tau_{sys}) \frac{df_{VCO}}{dt} \quad (\tau_0 = 2\Delta r/c \approx 2.4 \text{ ns})$$

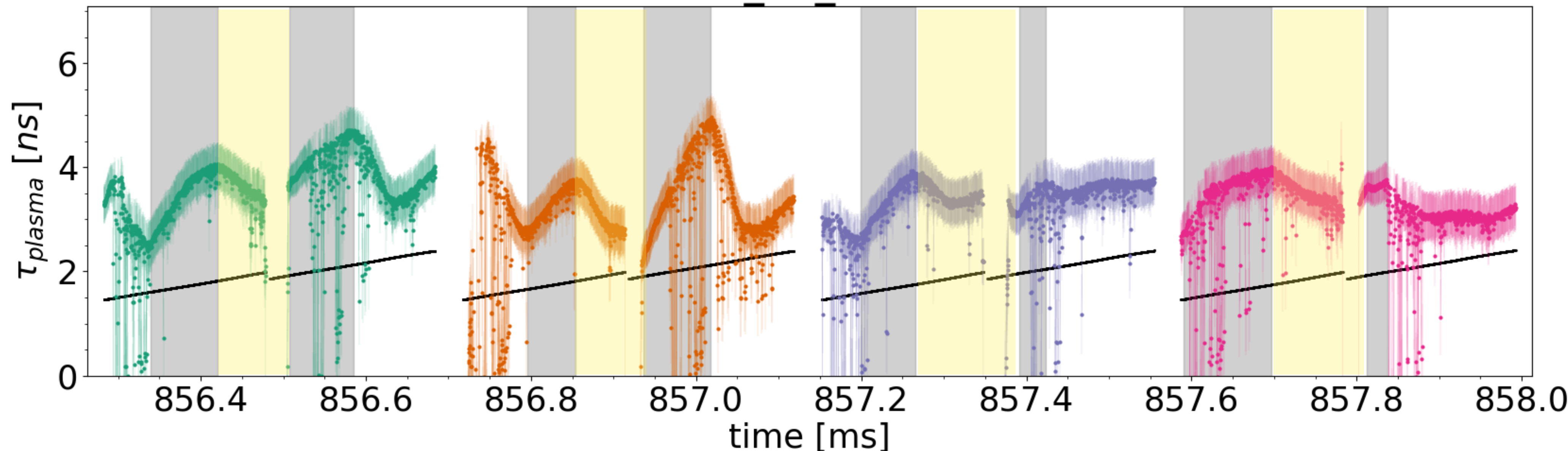




# Understanding of the delay time evolution during plasma operation



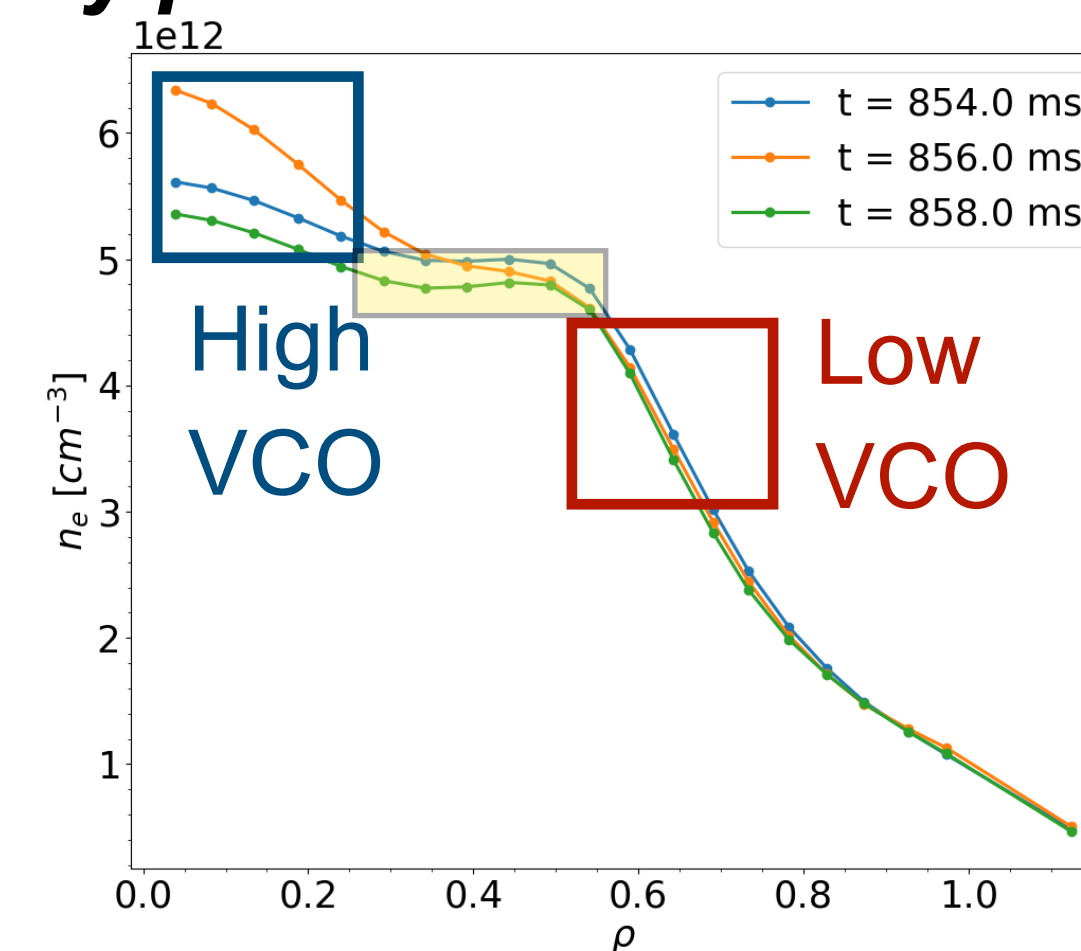
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Density profile from interferometer

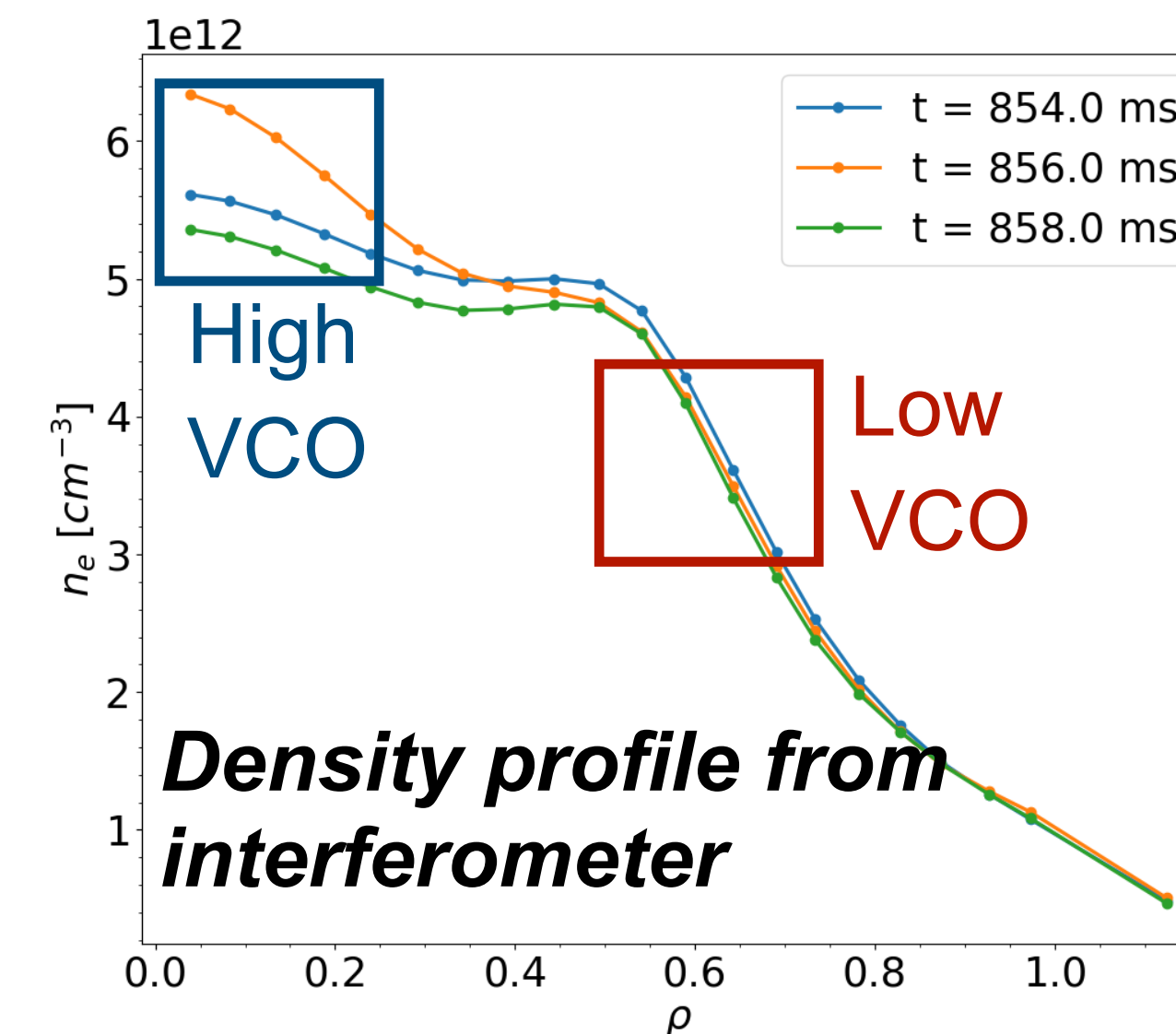
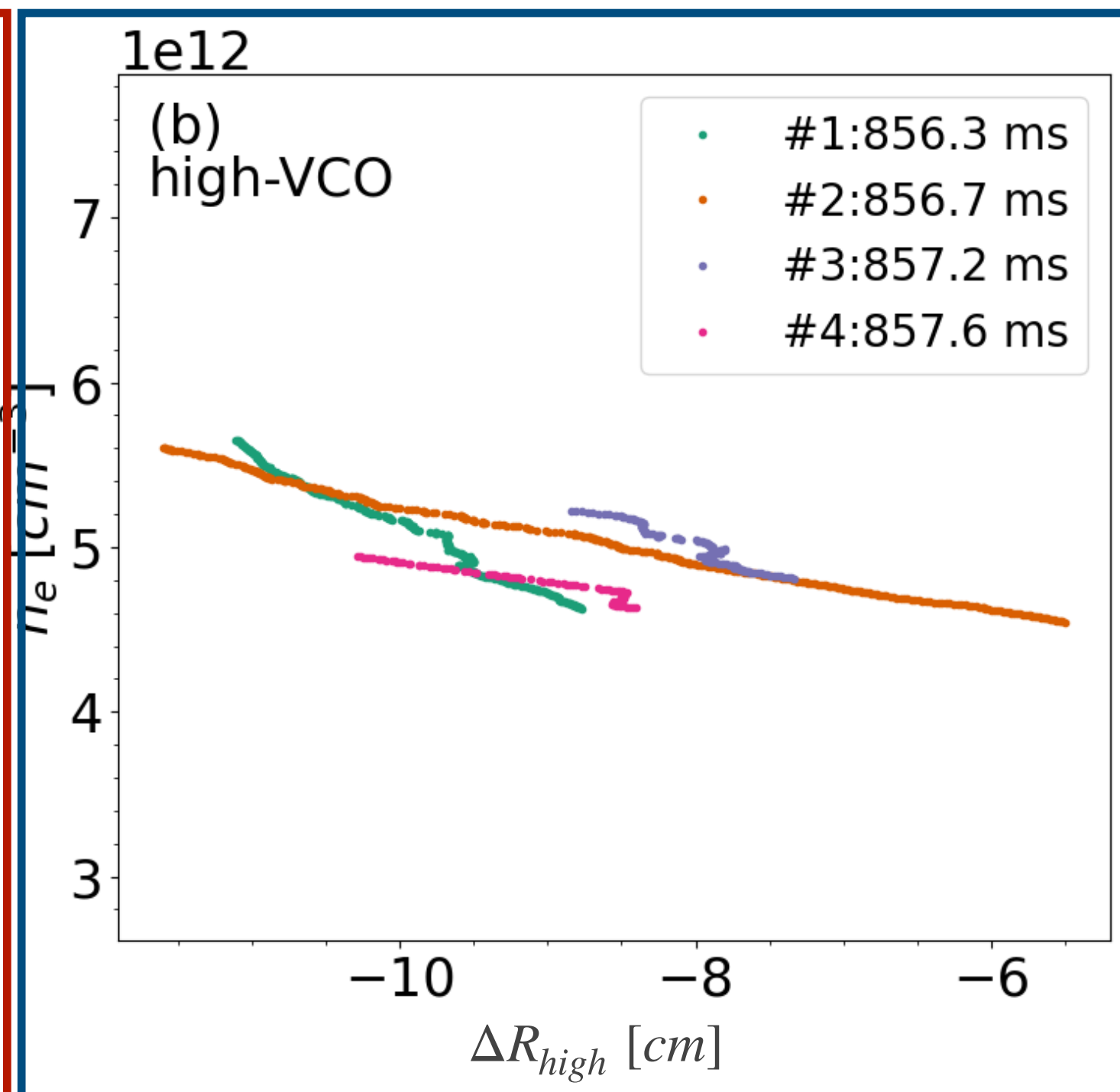
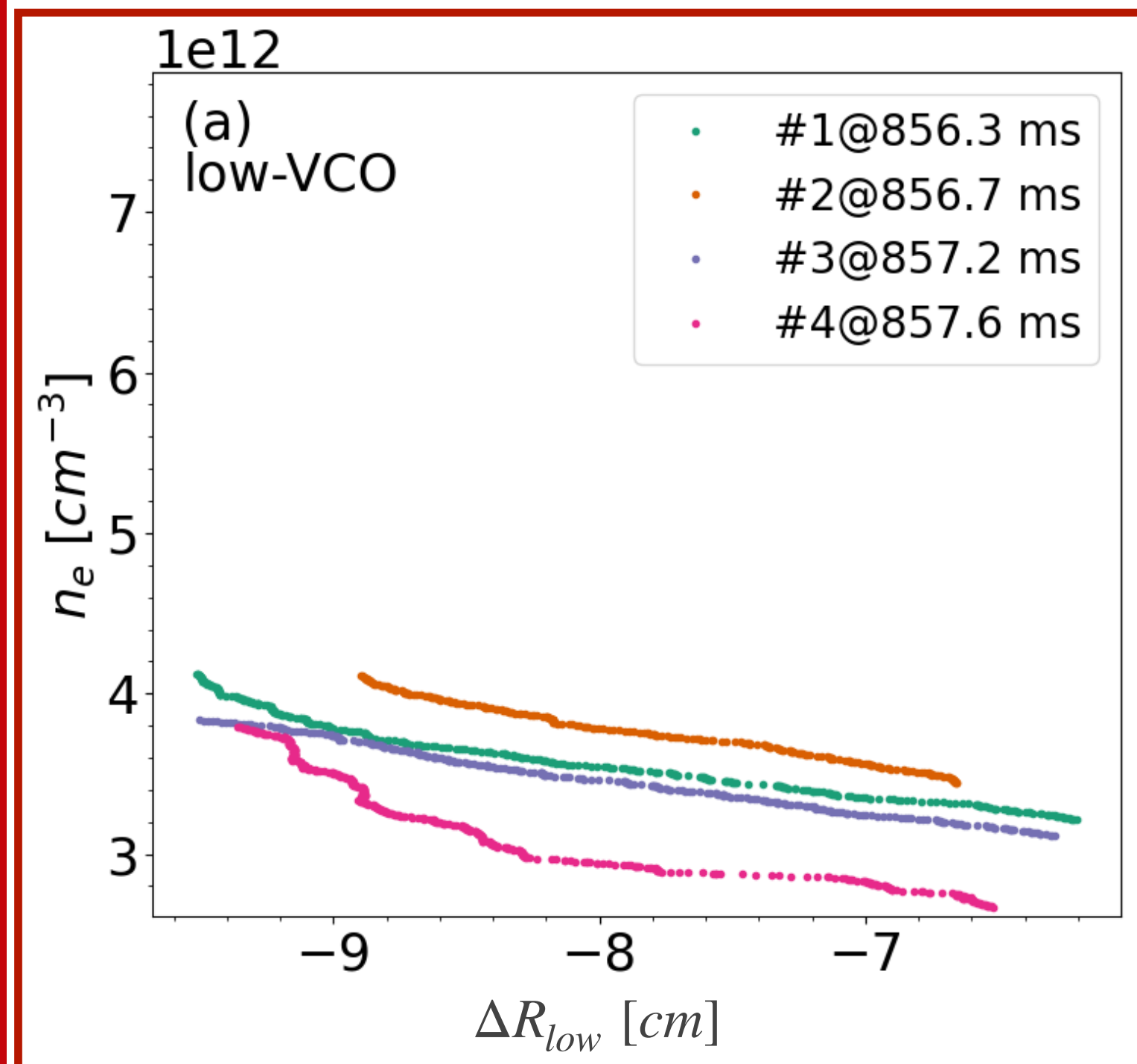
$$\tau_{plasma} = (f_{beat} - f_{beat,wall}) \left( \frac{df_{VCO}}{dt} \right)^{-1} + \tau_0$$

- **Low-VCO:** start from the positive slop
- **Blind area (yellow):** Neglect the  $d\tau/dt < 0$  between low- and high-VCOs
- **high-VCO:** select only the first phase with positive slop





# Abel integral is performed to obtain the relative cutoff position ( $\Delta R$ )



Abel integral is performed to calculate the cutoff position:

$$\Delta R = -\frac{c}{2\pi^2} \int_{f_0}^{f_c} \tau_{plasma} (f_c^2 - f^2)^{-0.5} df$$

- For O-mode, beat signal from low- and high-VCO is uncorrelated
- Density profile is obtained as a function of relative radius, consistent with the interferometer profile
- Mapping profile to major radius is ongoing, with the help of TS





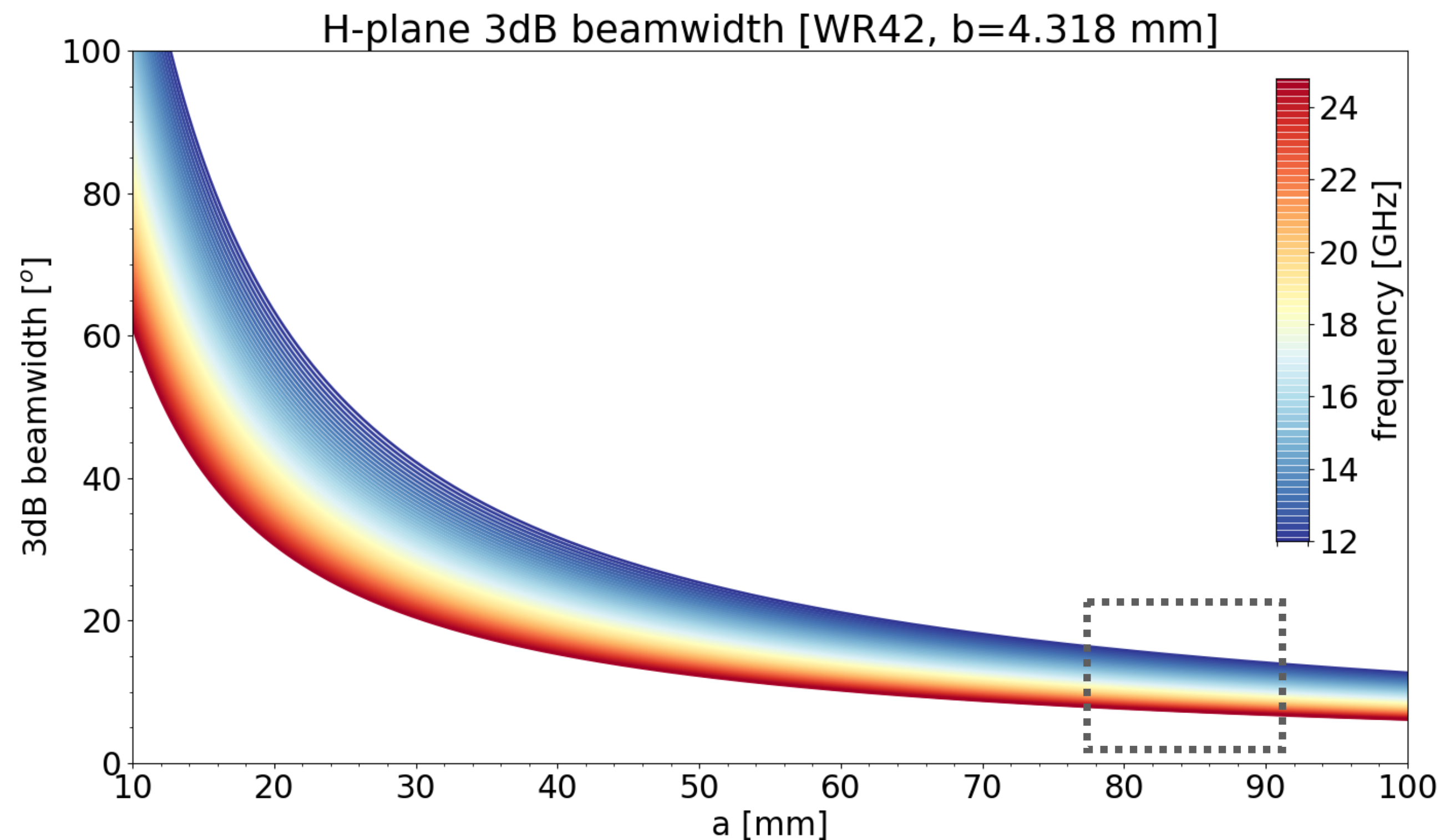
# Outline



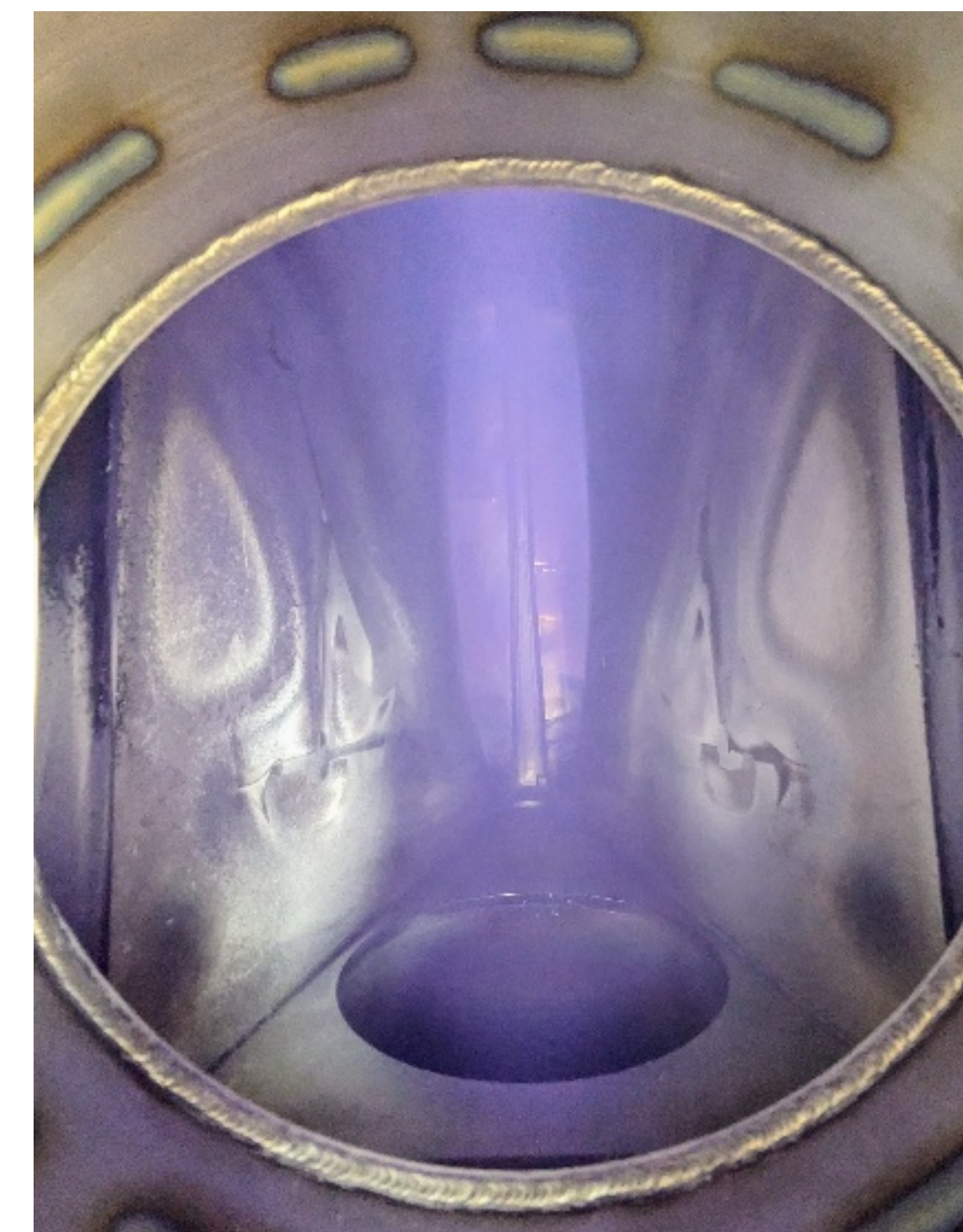
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# Replacing the antenna by a bi-static H-plane sectoral antenna pair



*plasma viewing window from  
the port of glow discharges*

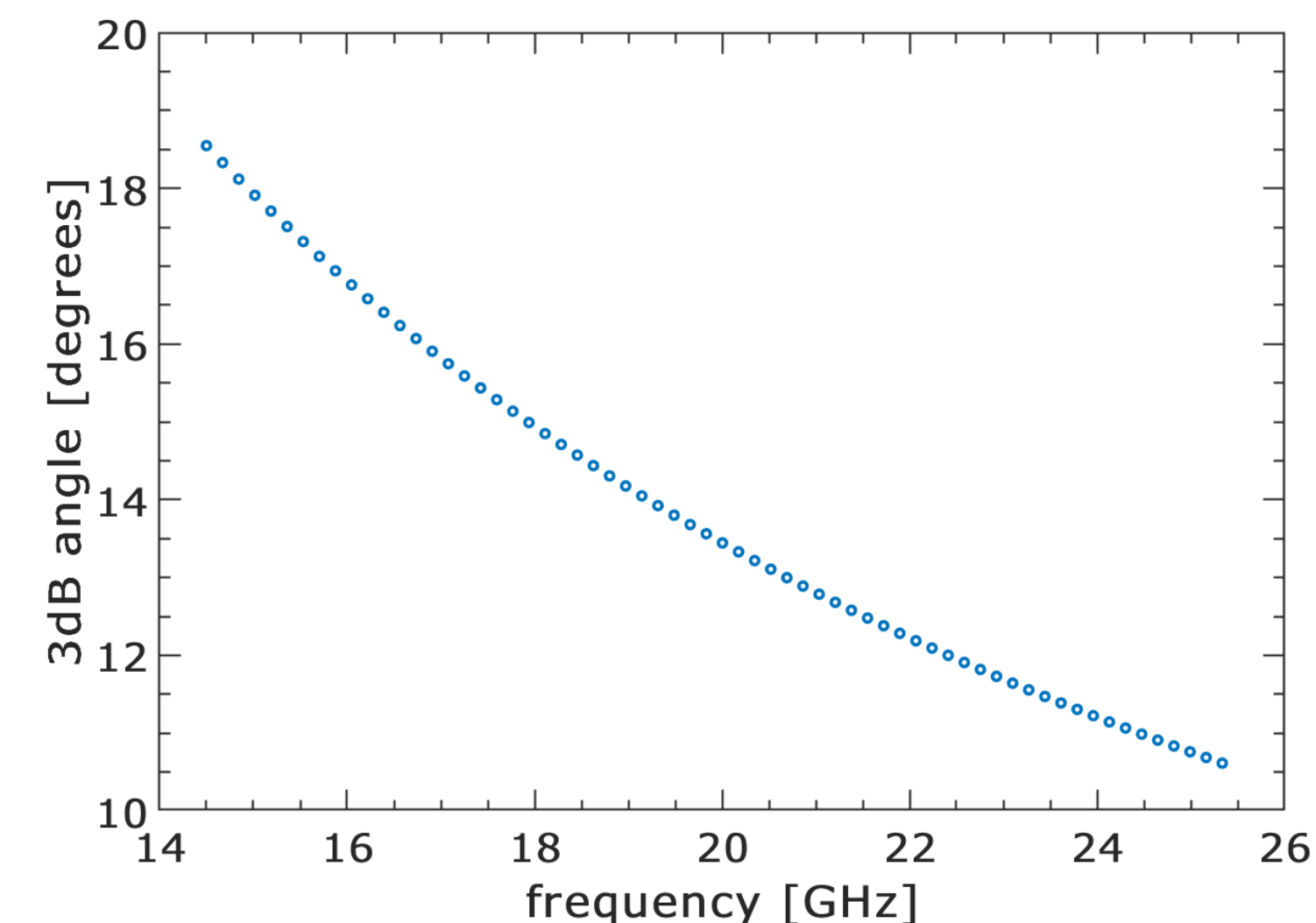
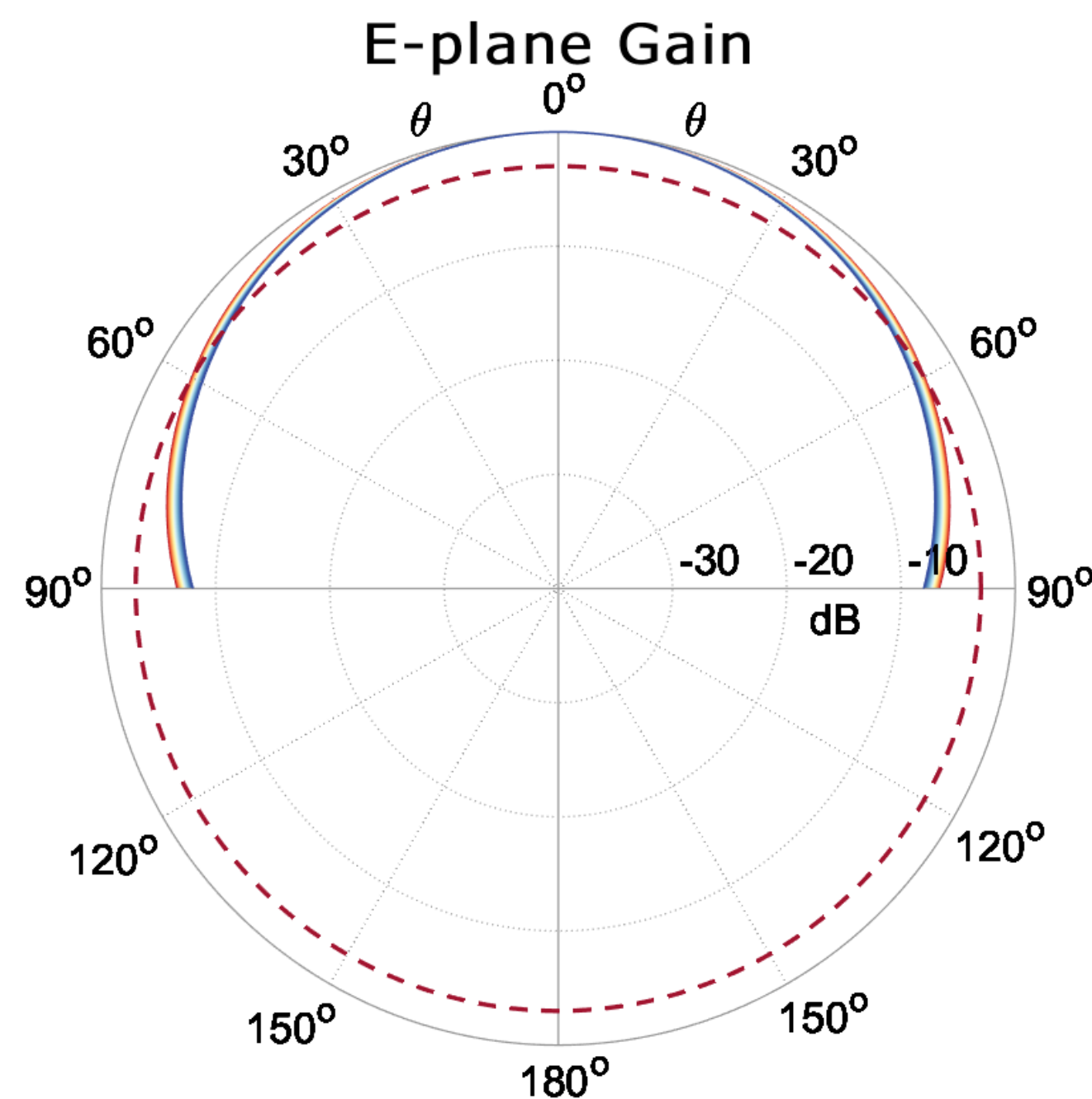
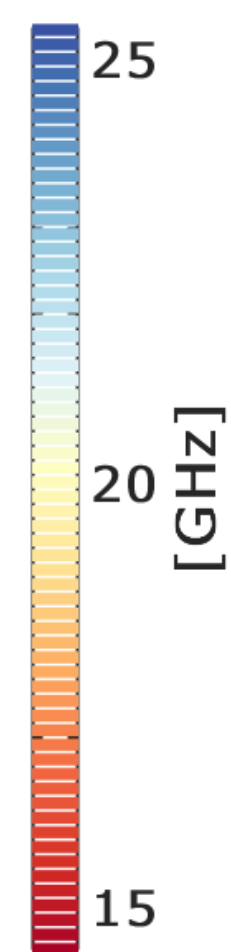
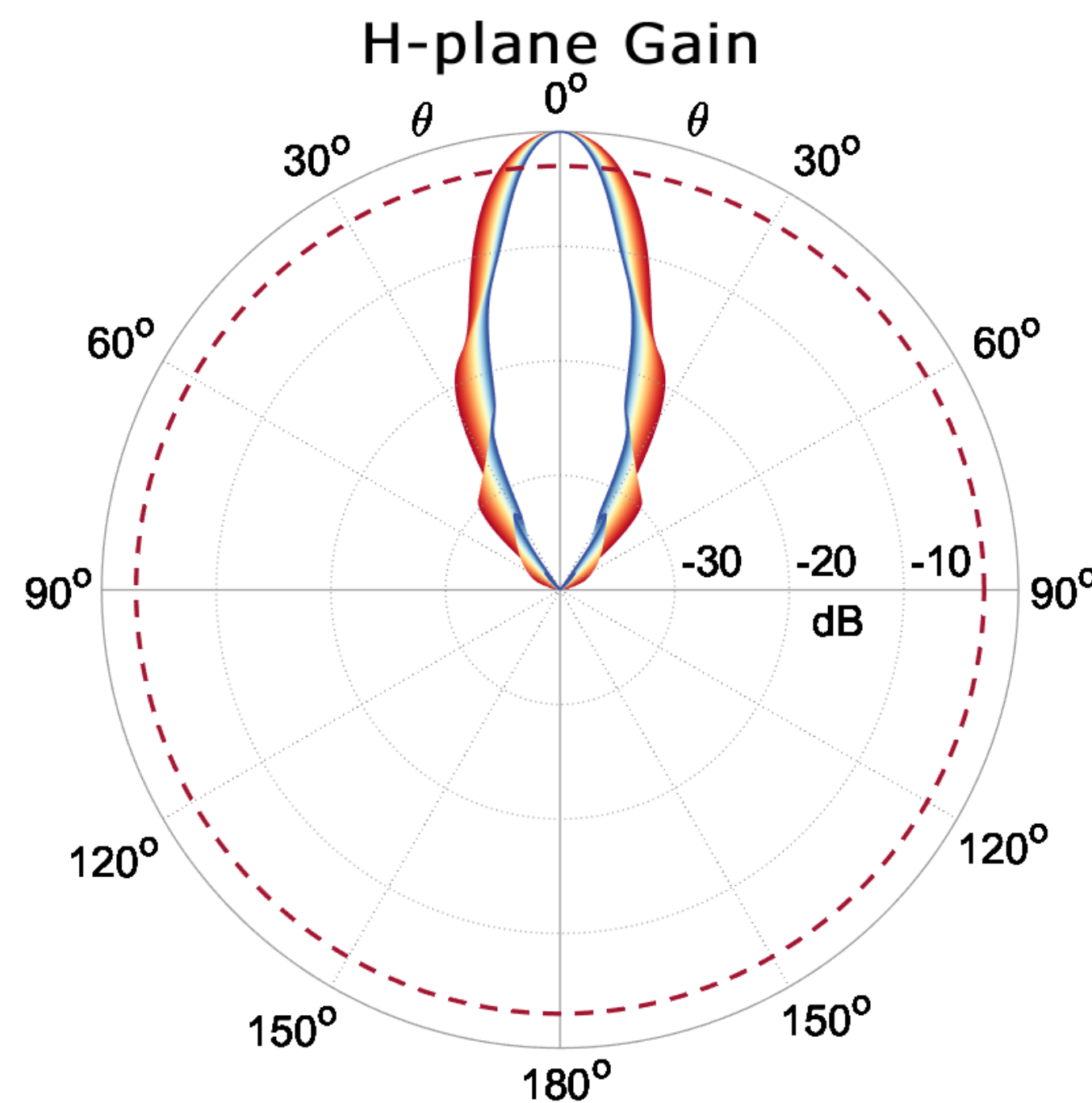


- Separate the Tx and Rx beam using a bi-static antenna pair
- Due to the limited space at the port, H-plane sectoral antenna pair is preferable
- Keep E-plane at 4.318 mm and extend the H-plane width of the antenna
- 80~90 mm of H-plane reduces the 3dB pattern below 20°





# Radiation pattern calculation indicates a finite beam width and gain

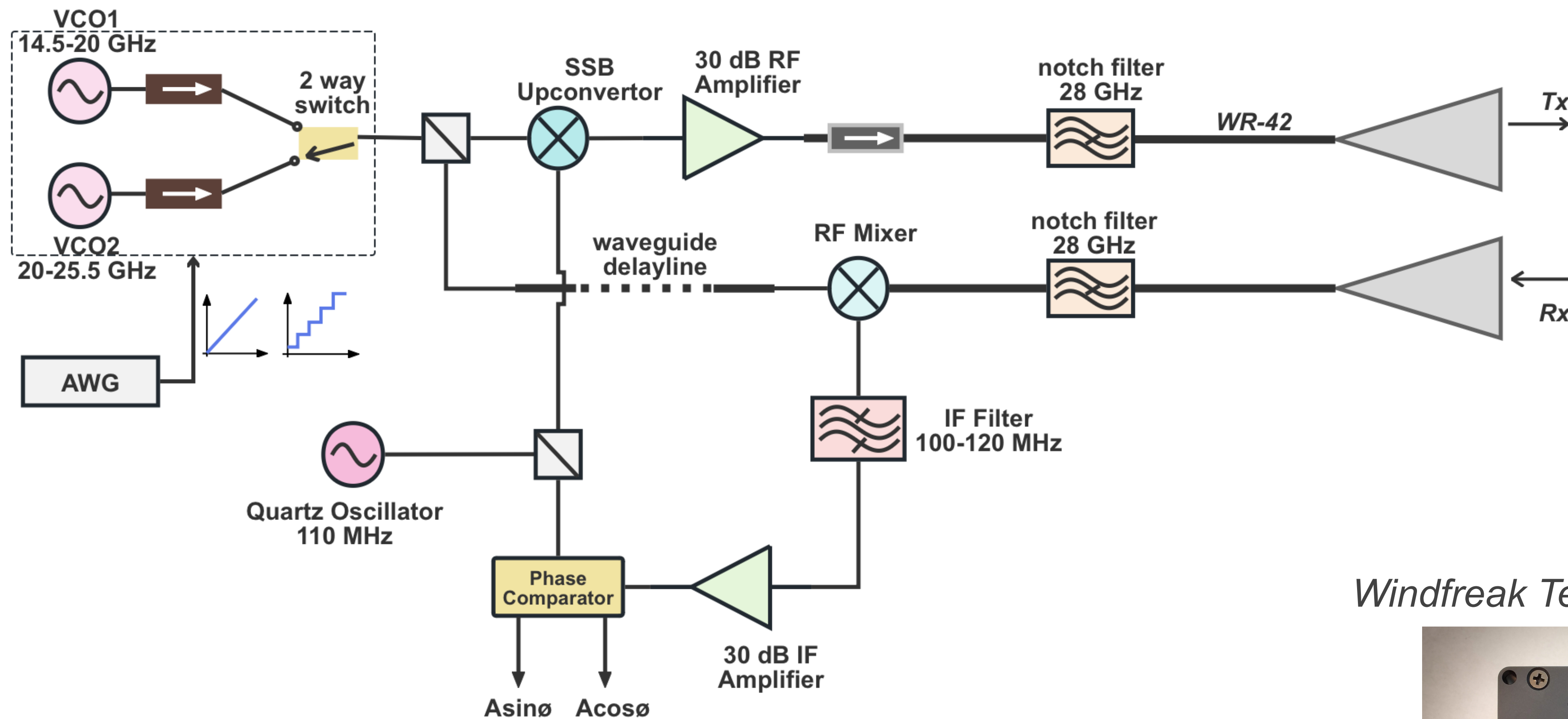


- H-plane sectoral antenna:  $a = 4.318$  mm,  $b = 88.5$  mm
- Frequency scan from 14.5 to 25.5 GHz
- H-plane beam width reduces as increasing the frequency
- Finite H-plane beam width, broadened in E-plane
- Future work: estimate the angle of viewing window, and compare with the beam width

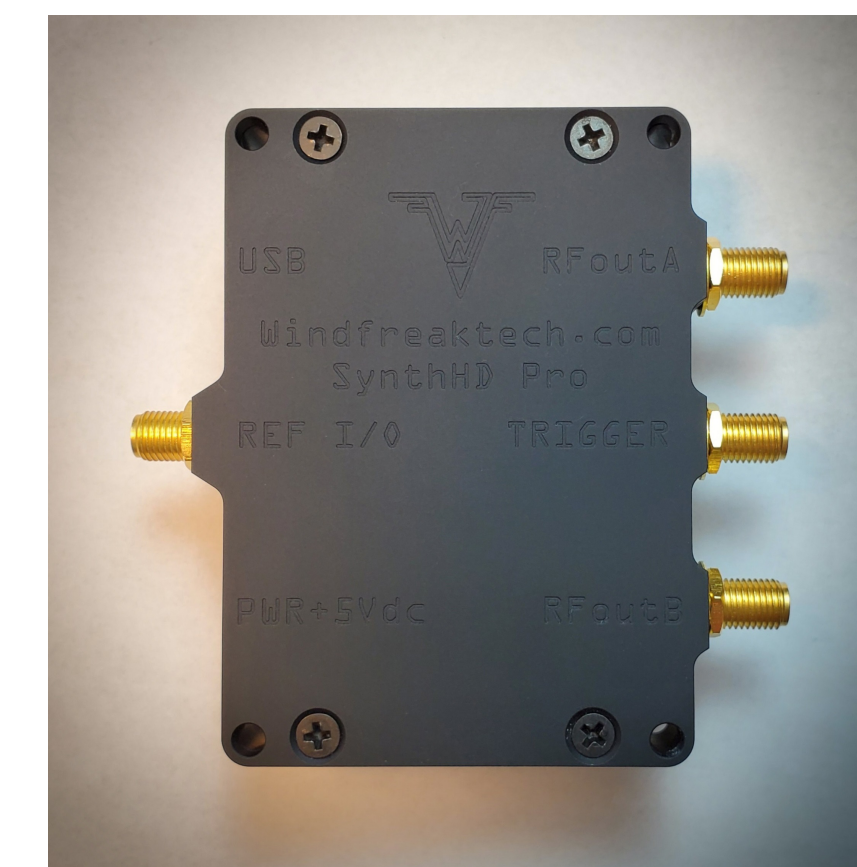
• *M. Richardson's talk for more details*



# Renovate the component layout to improve the system SNR



Windfreak Technologies, LLC



- Move the SSB and RF amplifier to the Tx branch
- Separated VCO signal to the RF mixer to reduce the noise at the LO
- Replace the VCO sources + switch by a broad band low-noise synthesizer
- ***M. Richardson's talk for more details***

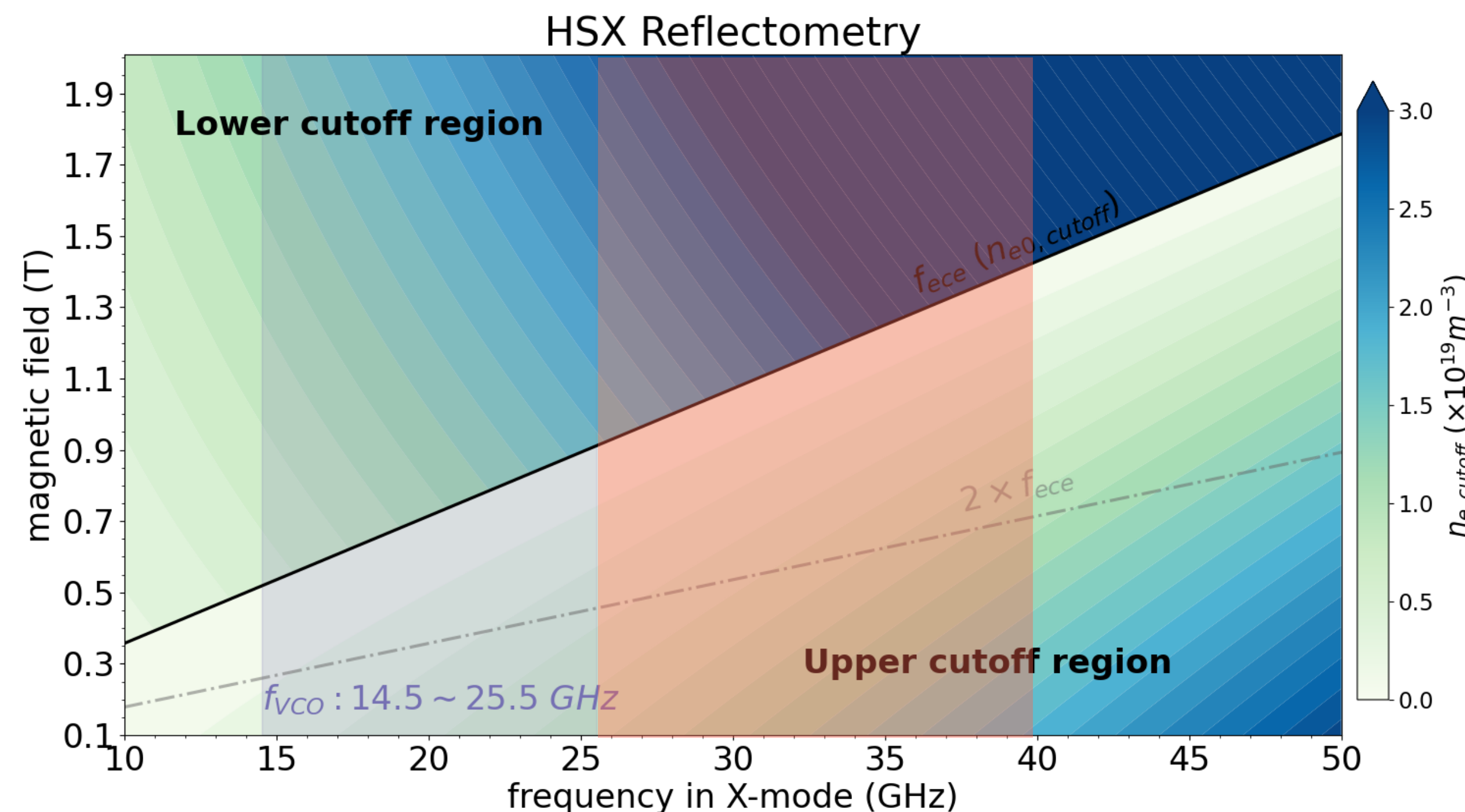




# Future plan on the system development



1. **Ka-band extension**: broaden the radial coverage, especially for X-mode (lower and upper cutoff regions, preferable for 1.25 T)
2. **Doppler reflectometry branch**: turbulent rotation and radial electric field measurements based on current regime and a rotatable mirror - see **M. Richardson's talk**
3. **Ray-tracing and full-wave simulation** - see **H. Miller's talk**
4. **Position reflectometry**: multi-poloidal positions for plasma shape measurement (monostatic, X-mode)
5. **synthetic reflectometry diagnostic**





# Summary



- HSX reflectometry is capable of measuring the density fluctuation and profile, and is flexible for 0.5 T and 1 T plasma operation by tuning the polarization between O- and X-mode
- Fluctuations at low frequency are observed during the resonant scan
- 100 kHz fluctuation is observed during the gas puffing modulation, responding to a density gradient change
- O-mode linear frequency scan is performed for profile inversion
- Relative density profile is obtained. Mapping to the major radius will be done with the help of TS
- Renovation plan includes: H-plane sectoral antenna pair, component layout modification, replacing the frequency source...
- A mirror rotation structure is designing, aiming for the Doppler reflectometry branch - see **M. Richardson's talk**
- Ray tracing is performed using Travis code for both angled (Doppler) and straight incident beam - see **H. Miller's talk**



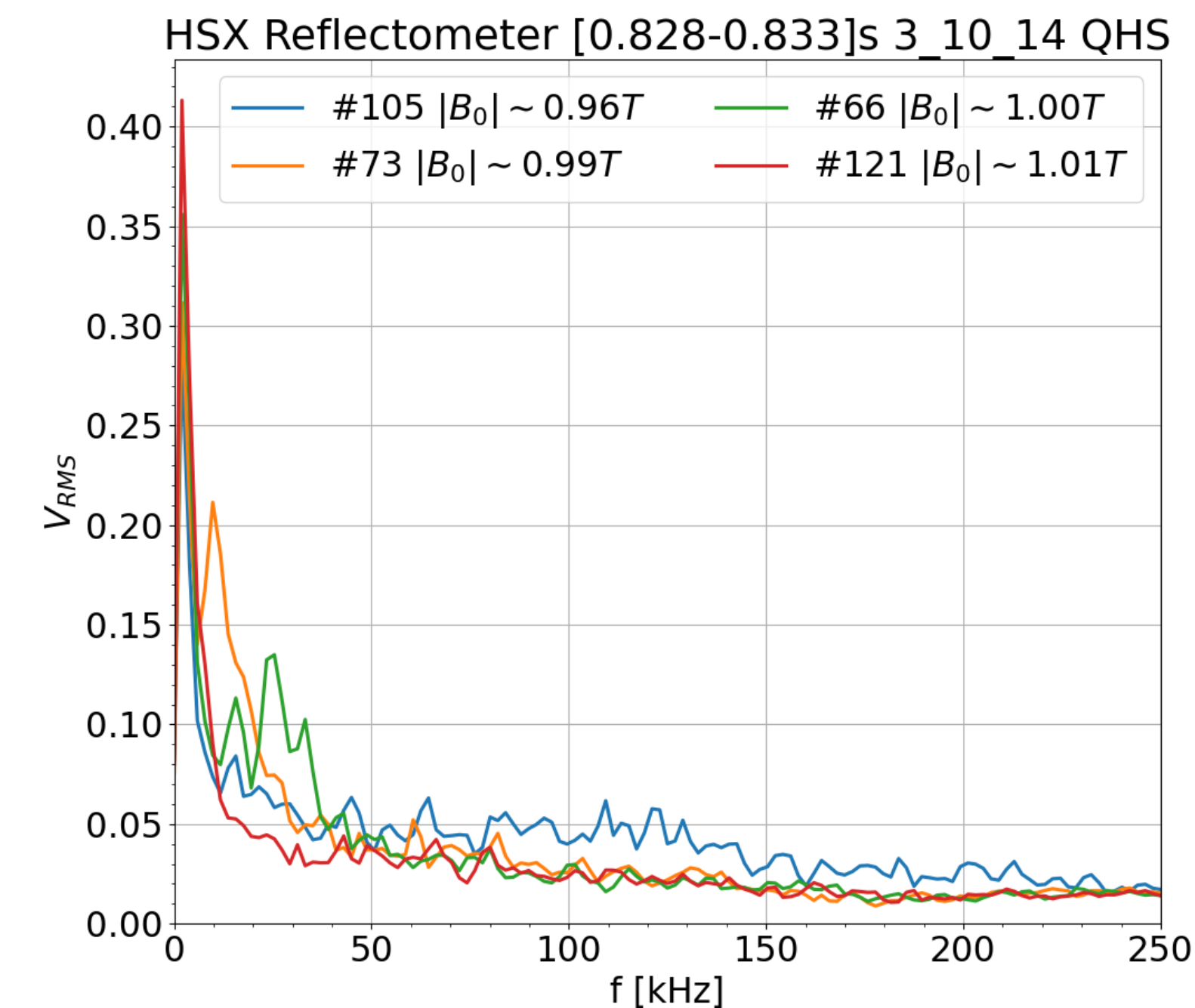
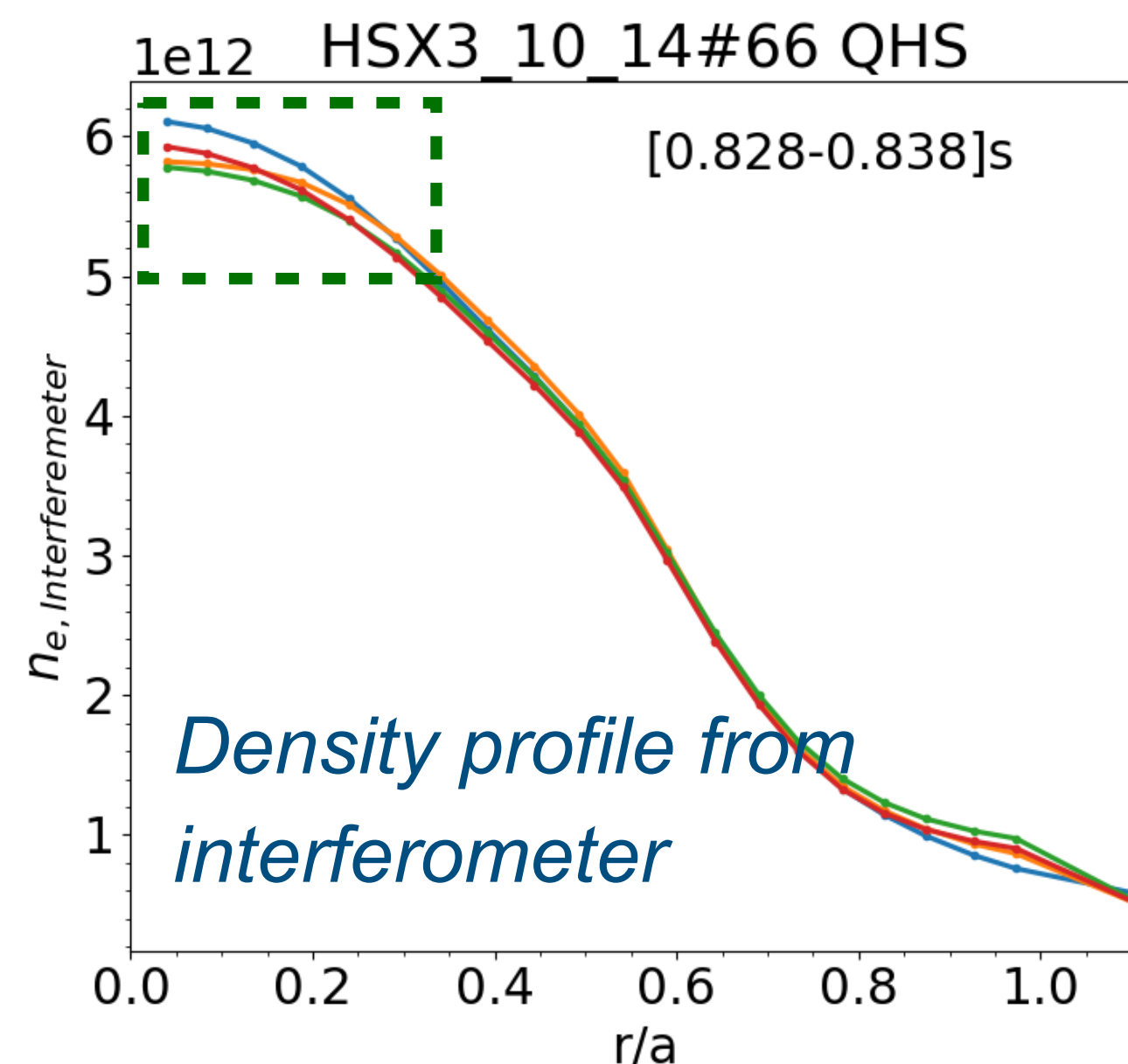
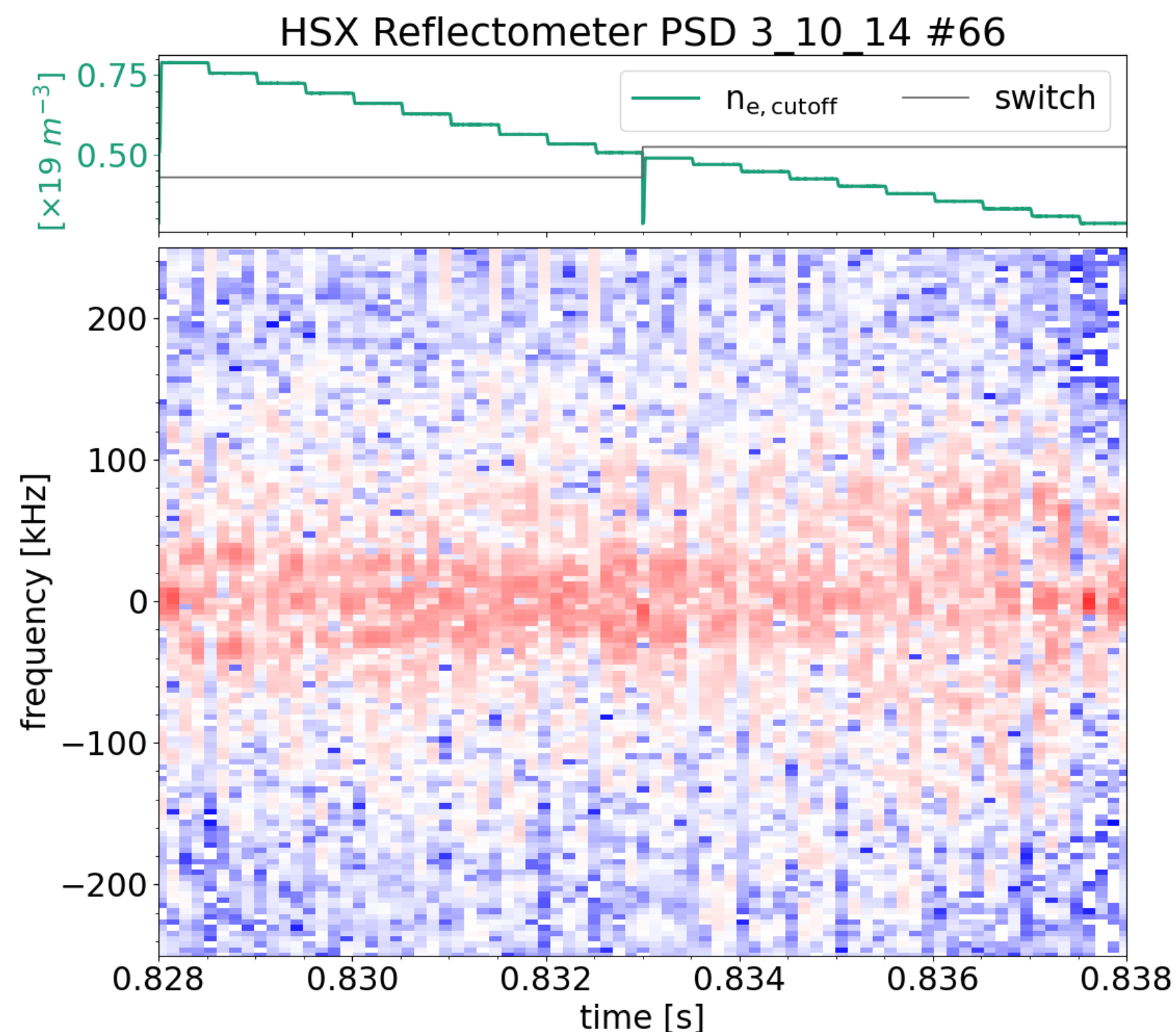


# Backup





# Low frequency mode appears in plasma core during the resonance scan



- Mode frequency 10~30 kHz at  $n_{e,cutoff} > 0.5 \times 10^{19} m^{-3}$
- Core-localized mode. Radial position of the mode is confirmed from the interferometer
- $f = 10$  and  $30$  kHz with on-axis heating (#66, #73)
- Broadband fluctuation at 50-150 kHz rises with outboard-side heating (#105)
- No clear mode observed at inboard side heating (#121)

G Weir, PhD thesis